A close-up photograph of several large, light-colored structural hollow sections (tubes) arranged in a complex, overlapping pattern. The tubes are connected by welded joints, and the background shows a corrugated metal surface.

# **Specification of Structural Hollow Sections & Welded Joints In Tubular Steel**

**Steve Whitfield Beng (Hons) CEng MStructE**  
**Customer Technical Services - Manager**

# Tata Group

One of the world's fastest-growing and most reputable corporations



## Tata Group is highly diversified

- Steel , Consultancy , Automotive , Power , Communications , Hotels . beverages
- Operations in more than 100 countries and 580,000 employees
- Total revenues \$100 billion (67% from outside India)
- Ranked world's 11<sup>th</sup> most reputable and 17<sup>th</sup> most innovative company
- Tata Sons 66% owned by philanthropic trusts
- £170 million invested in community projects last year

## Tata Steel Group

One of the world's most geographically-diversified steel producers

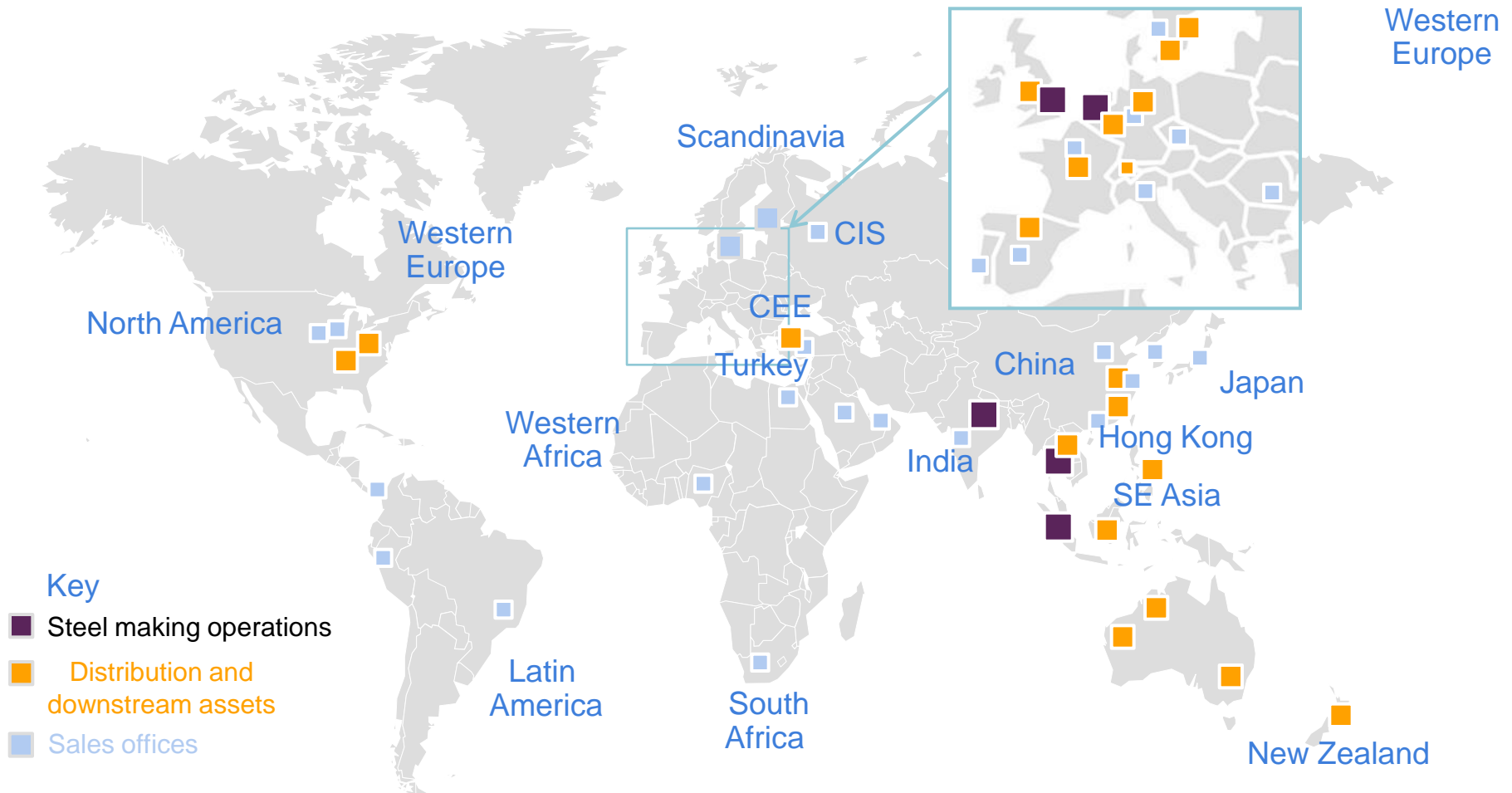


### Tata Steel Group

- Top 12 global steel producer
- Annual crude steel capacity of more than 29 million tonnes
- Around 80,000 employees
- Manufacturing operations in 26 countries across 4 continents
- Present in both mature and emerging markets
- Turnover in 2013-14: \$ 24.8 billion (€18.0 billion)
- Fortune 500 company

# Tata Steel Group

A global network serving demanding markets worldwide





# Our key markets

Serving the most demanding markets worldwide

**Aerospace**



**Automotive**



**Construction**



**Consumer products**



**Defence & security**



**Energy & power**



**Lifting & excavating**



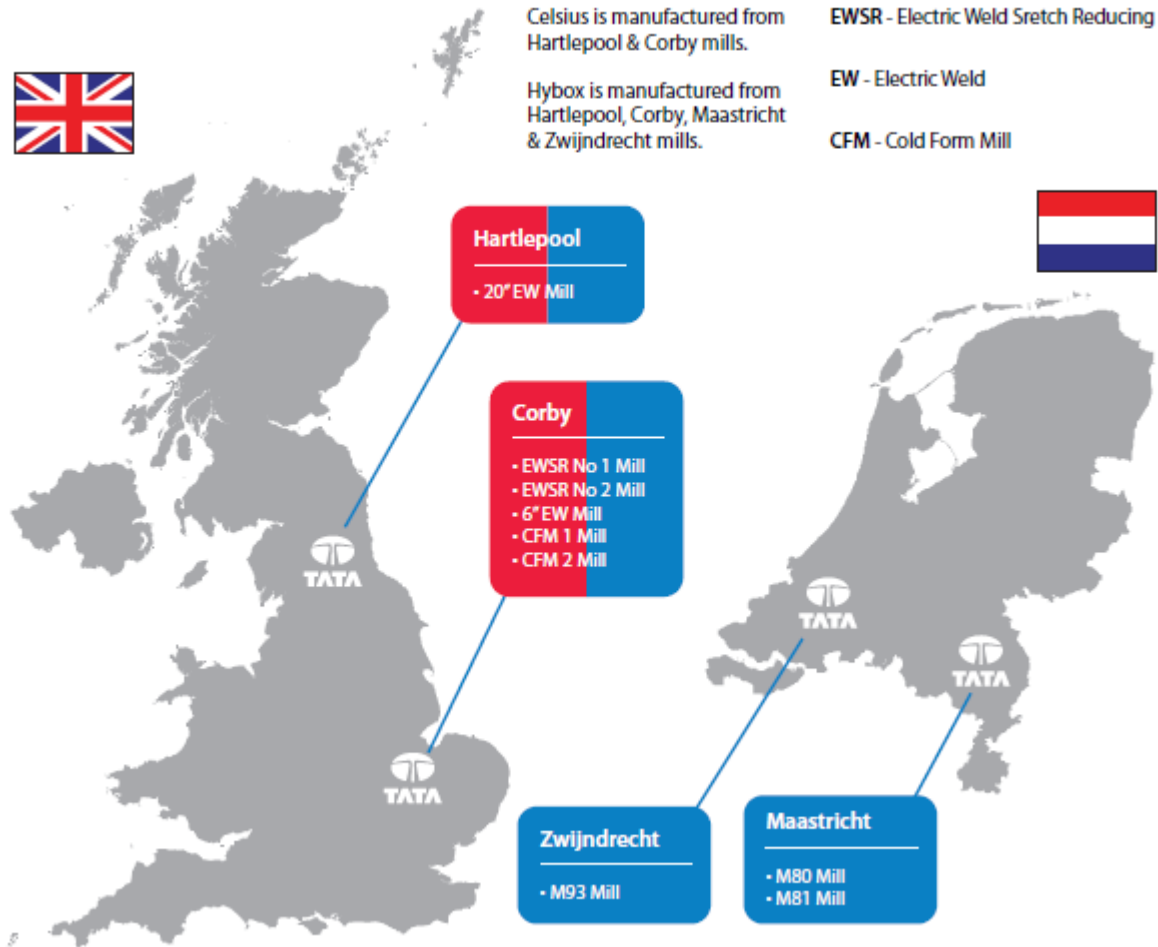
**Packaging**



**Rail**



## Tata Steel – Tube manufacturing



# **Tata Steel Europe, Tubes**

**Celsius – EN10210 Hot finished Structural Hollow Sections**

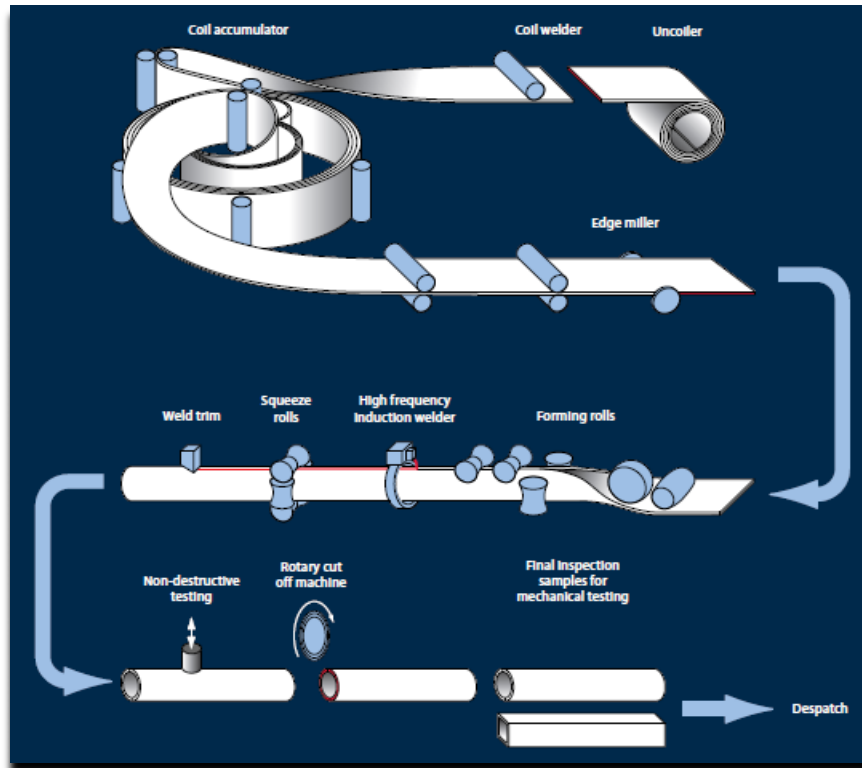
**Steve Whitfield Beng (Hons) CEng MStructE**  
**Customer Technical Services - Manager**

# Tata Steel Europe, Tubes

**1****Technical information****2****Testing, Certification and traceability****3****Technical Support & Tools****4****Summary**

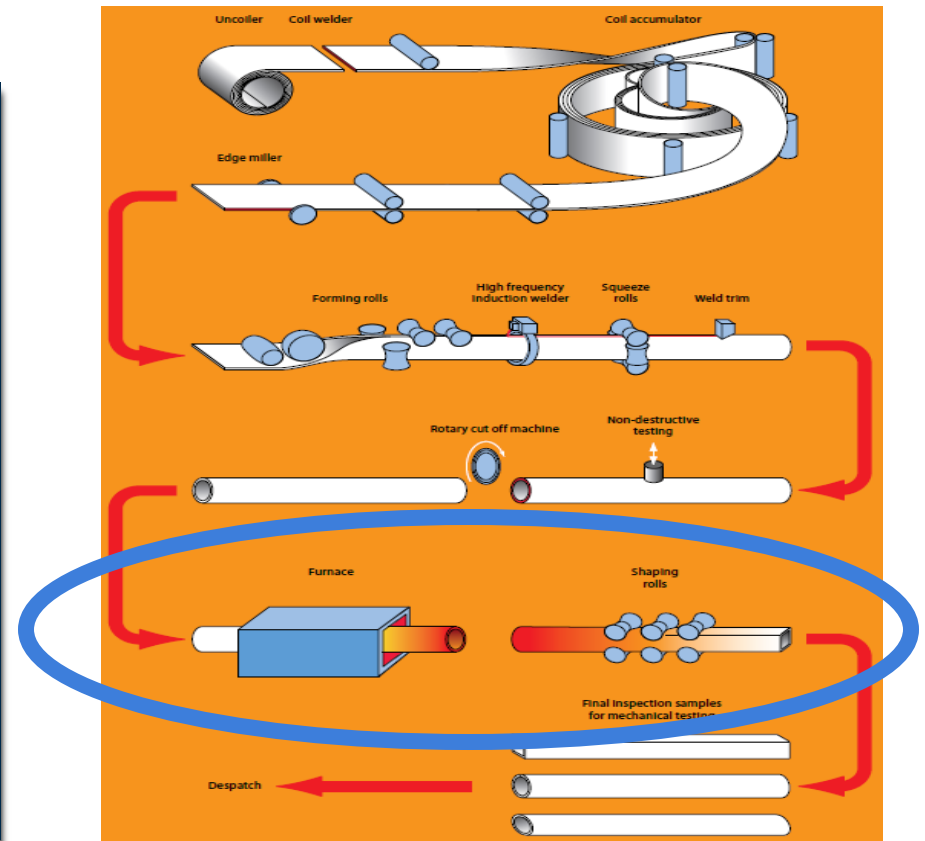


# Manufacture of Hollow Sections



**EN10219 – Cold Formed Structural Hollow Sections**

**Hybox**

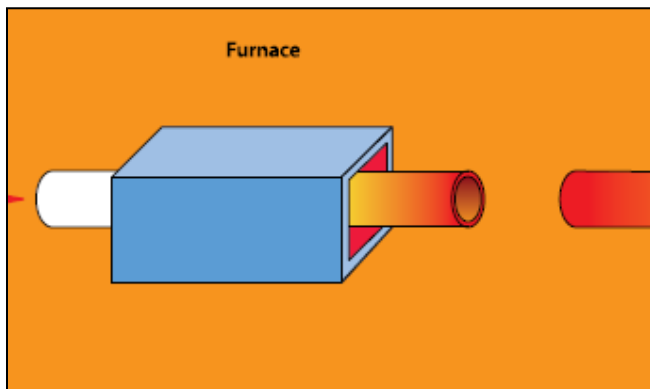
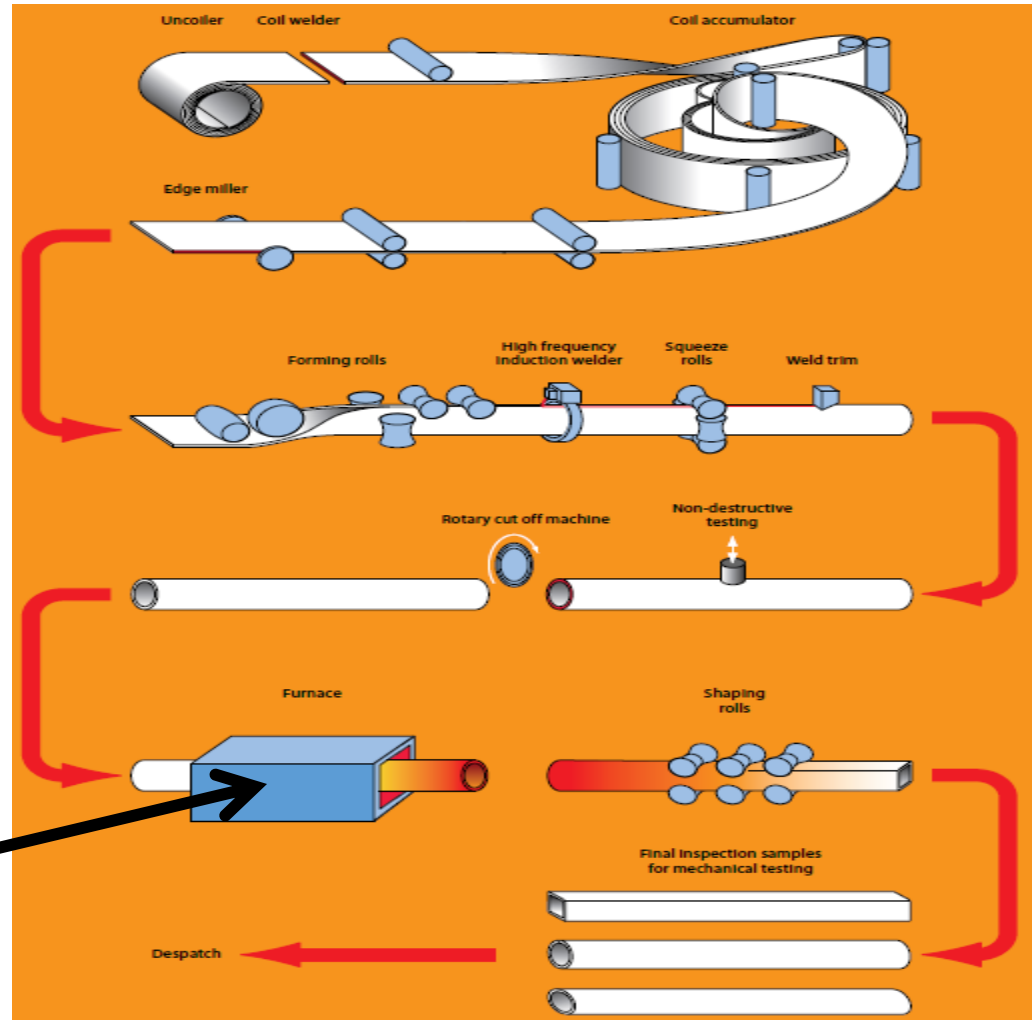
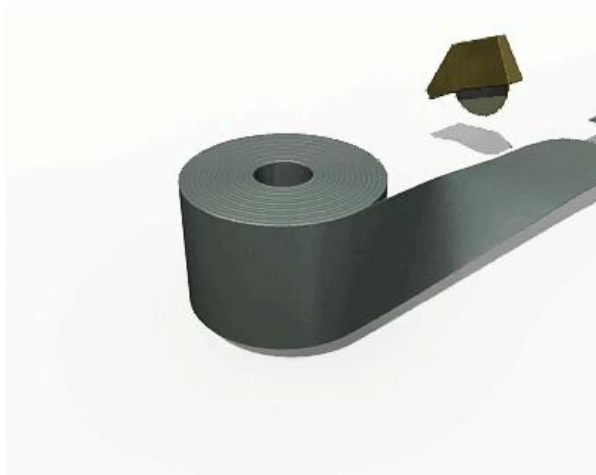


**EN10210 – Hot Finished Structural Hollow Sections**

**Celsius**

## Technical Information

Celsius 420 – Full Body  
Normalised



**Furnace**

## The right product for the right application

### Hot Finished Structural Hollow Sections

- EN10210:S355 NH, EN10210:S355J2H
- EN10210:S420 NH

### Cold Formed Structural Hollow Sections

- EN10219:S355J2H
- EN10219:S355JRH

It is important to ensure you have the correct specification

## Technical Information

Hot Finished Structural Hollow Section of Non alloy and Fine Grain Steels

# CELSIUS 355 - EN10210:S355 NH

Tensile Strength  
470N/mm<sup>2</sup> – 630 N/mm<sup>2</sup>

Minimum yield strength  
≤ 16mm :- 355 N/mm<sup>2</sup>

Minimum Impact -20°C @ 40 J

Elongation - 19 %

Carbon Equivalent (CEV)  
– 0.43

Silicon Content Si  
- 0.60

**Silicon Content (Si)  
Celsius 420 NH –  
0.15 to 0.25**

## Product Specification

## Technical Information

Hot Finished Structural Hollow Section of Non alloy and Fine Grain Steels

# CELSIUS 420 - EN10210:S420 NH

Tensile Strength  
520N/mm<sup>2</sup> – 680 N/mm<sup>2</sup>

Minimum yield strength  
≤ 16mm :- 420 N/mm<sup>2</sup>

Minimum Impact -20°C @ 40 J

Elongation - 19 %

Carbon Equivalent (CEV)  
– 0.50

Silicon Content Si  
- 0.60

**Carbon Equivalent  
(CEV)  
Celsius 420 NH – 0.45**

**Silicon Content (Si)  
Celsius 420 NH –  
0.15 to 0.25**

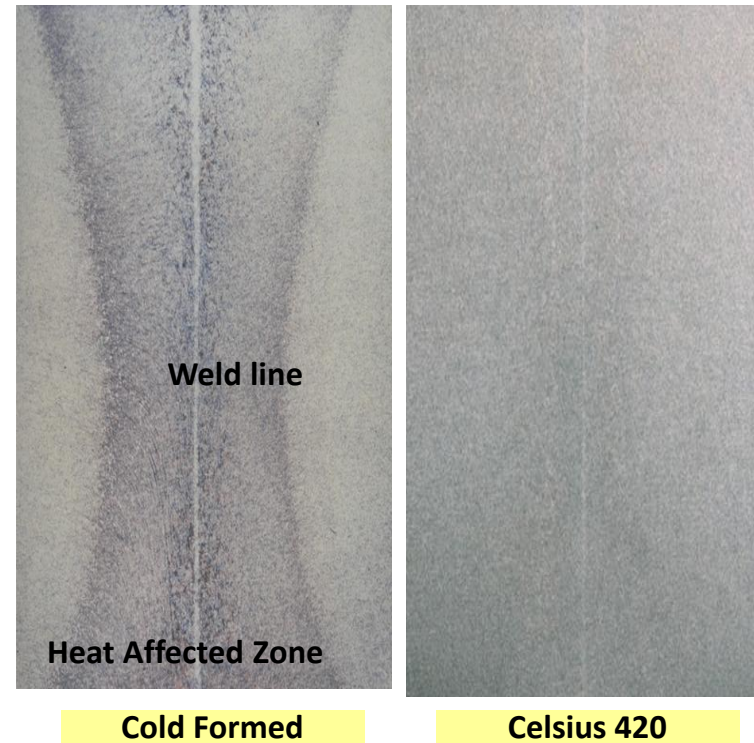
## Product Specification



## Technical Information

Due to the manufacture the Celsius has many advantages on a size for size basis compared to EN10219:

- Tighter corner profiles on hot. – Better area less weight.
  - Weld line - Due to the full body normalising the weld line becomes the same as the tube. Better consistency for product
- Consistent hardness values around the whole perimeter. – During heating or manipulating/ bending no loss of yield, tensile, Charpy impacts. Can weld in corner of hot but issues with cold.
- No built in stress – Design standards recognise the difference and have higher compression and tension for same size same thickness.



Advantages of Celsius Compared to Cold Formed

## Technical Information

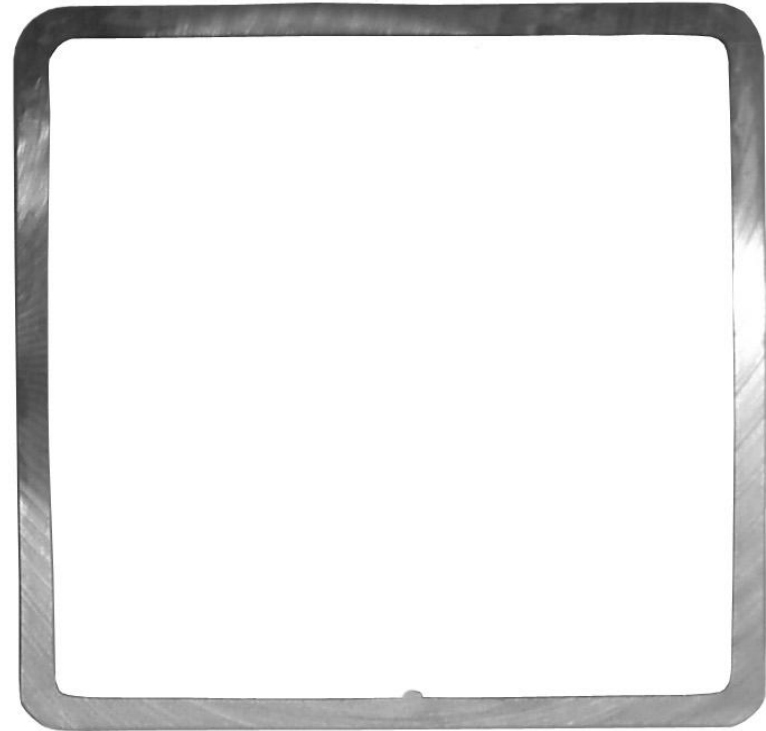
**EN10219 Cold Formed products**

**Hybox**



**EN10210 Hot Finished products**

**Celsius**



**Advantages of Celsius Compared to Cold Formed**

## Technical Information

### Comparison Hot and Cold for design - Sectional properties

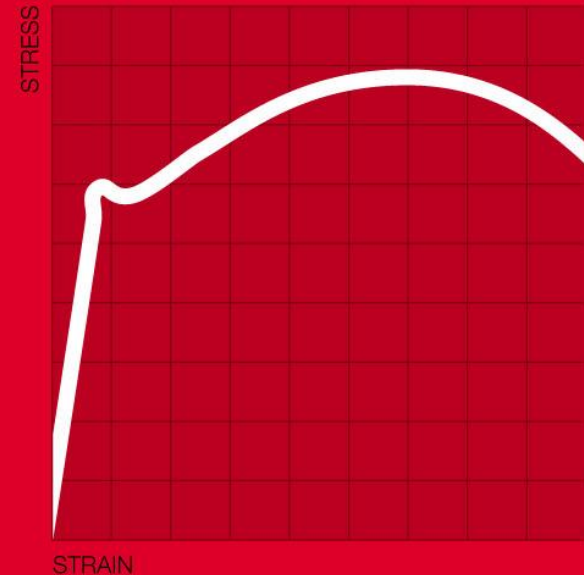
EN10210 Hot finished EN 10219 Cold formed	Area(A) cm <sup>2</sup>	Moment of Inertia(I) cm <sup>4</sup>	Elastic modulus(Z) cm <sup>3</sup>
120 x 120 x 8 RHS Hot Finished	35.2	726	121
120 x 120 x 8 RHS Cold Formed	33.6	677	113

Advantages of Celsius Compared to Cold Formed

## Mechanical properties

### Hot finished

- Test results follow normal load extension characteristics with clear indication of yield strength.
- Gives the recommended ratio of yield to ultimate strength-0.84 maximum.
- High ductility-adequate warning of dangerous overload condition indicated by excessive deformation.



Hot finished. Tensile test taken  
from flat side – Hot finished sections  
uniform across the section

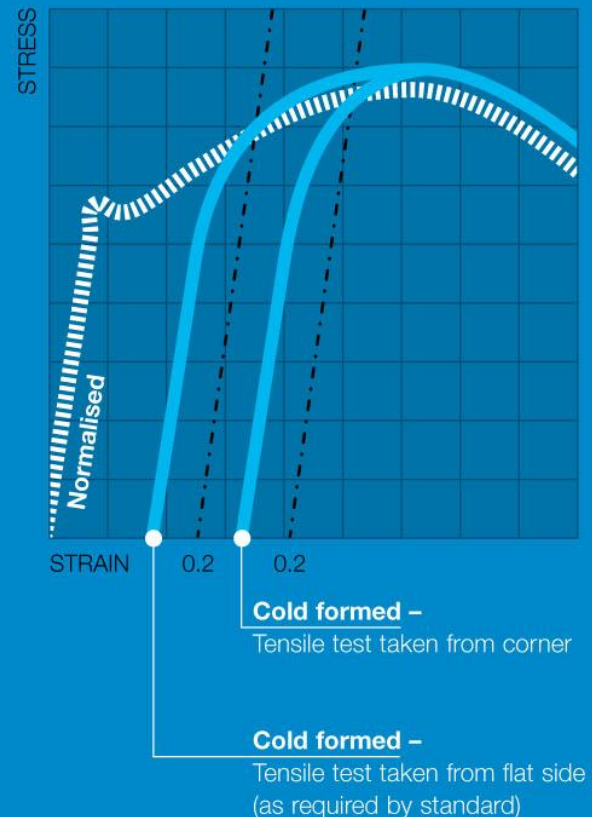
**Advantages of Celsius Compared to Cold Formed**

## Mechanical properties

### Cold formed

- Test results differ in samples taken from corners and flat sides.
- There is no clear yield point-0.2% proof stress is normally quoted for yield strength.
- Increase in ratio of yield to ultimate strength-may be above that recommended by design standards.
- Lower ductility-less visible warning of dangerous overload condition possibility of brittle fracture.

Effect of Cold working  
(Taken from typical tensile tests)



## Advantages of Celsius Compared to Cold Formed

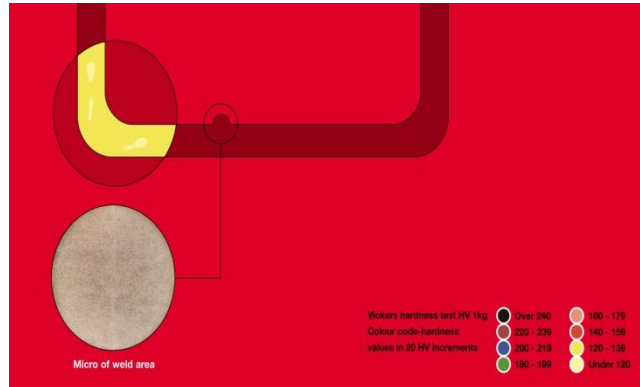


## Comparison of strut capacity (kN) EC3

	$\lambda$ bar	Hot finished S355J2H	Cold formed S355J2H	CF/HF Difference
120x120x5	0.8	641	526	0.82
120x120x10	0.8	1212	954	0.78
300x300x12.5	0.8	4011	3103	0.75
406.4 x 16	0.8	5536	4607	0.83

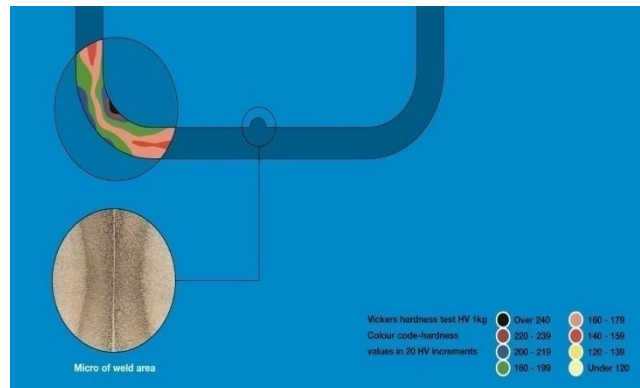
Advantages of Celsius Compared to Cold Formed

# Structure & Hardness



## Hot Finished products

- Uniform grain structure and hardness values
- Mechanical properties are stable and uniform across the whole section



## Cold Formed products

- Varying grain structure and hardness values, particularly in the corners and seam weld area
- Mechanical properties vary across the section

**Advantages of Celsius Compared to Cold Formed**

#### 4.14 Welding in cold-formed zones

- (1) Welding may be carried out within a length  $5t$  either side of a cold-formed zone, see Table 4.2, provided that one of the following conditions is fulfilled:
- the cold-formed zones are normalized after cold-forming but before welding;
  - the  $r/t$ -ratio satisfy the relevant value obtained from Table 4.2.

**Table 4.2: Conditions for welding cold-formed zones and adjacent material**

r/t	Strain due to cold forming (%)	Maximum thickness (mm)		
		Generally		Fully killed Aluminium-killed steel (Al $\geq 0,02$ %)
		Predominantly static loading	Where fatigue predominates	
$\geq 25$	$\leq 2$	any	any	any
$\geq 10$	$\leq 5$	any	16	any
$\geq 3,0$	$\leq 14$	24	12	24
$\geq 2,0$	$\leq 20$	12	10	12
$\geq 1,5$	$\leq 25$	8	8	10
$\geq 1,0$	$\leq 33$	4	4	6

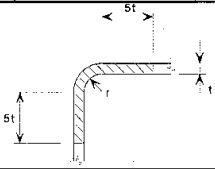
  


Diagram illustrating the cold-formed corner joint. The diagram shows a corner of a section with thickness  $t$ . The distance from the corner to the weld line is indicated as  $5t$ .

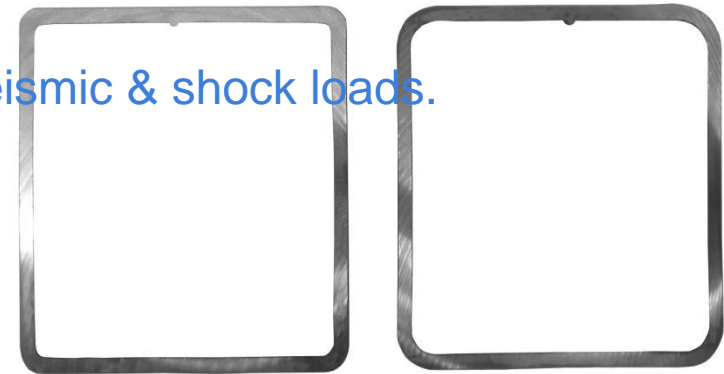
**NOTE** Cold formed hollow sections according to EN 10219 which do not satisfy the limits given in Table 4.2 can be assumed to satisfy these limits if these sections have a thickness not exceeding 12,5 mm and are Al-killed with a quality J2H, K2H, MH, MLH, NH or NLH and further satisfy  $C \leq 0,18\%$ ,  $P \leq 0,020\%$  and  $S \leq 0,012\%$ .

In other cases welding is only permitted within a distance of  $5t$  from the corners if it can be shown by tests that welding is permitted for that particular application. **AC2**

Eurocode  
EC3-1-8 table 4.2  
(including corrigenda  
feb 2010)

## Comparison between Hot & Cold

- Hot Finished Celsius - has no residual stresses from manufacturing.
- Hot Finished Celsius - has uniform grain structure and hardness
- Hot Finished Celsius - has tighter corner profile (2T max – Celsius).
- Hot Finished Celsius - has higher geometric properties.
- Hot Finished Celsius - has higher load capacity.
- Hot Finished Celsius - is fully weldable at corners
- Hot Finished Celsius - has superior ductility for seismic & shock loads.
- Hot Finished Celsius - has greater fire resistance.



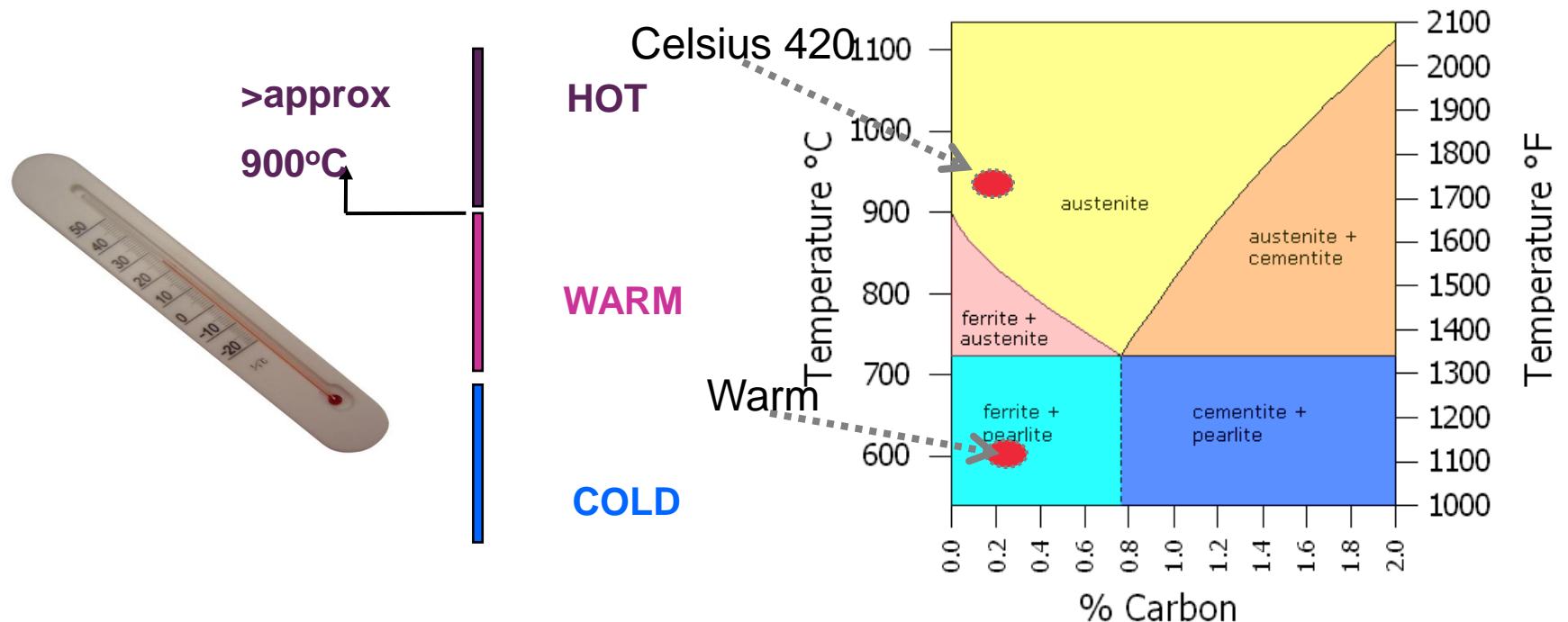
**Advantages of Celsius Compared to Cold Formed**

## Technical Information

The Celsius 420 is full body normalised and final shaped at a high temperature ensuring that the product is fully stress relieved.

The product Standard EN10210 does allow for warm/ stress relieved which will not give the same consistent values as Celsius.

The warm product is manufactured cold then shaped giving similar disadvantages for manufacture as the cold product



**Advantages of Celsius Compared to Warm/ Stress relieved products**

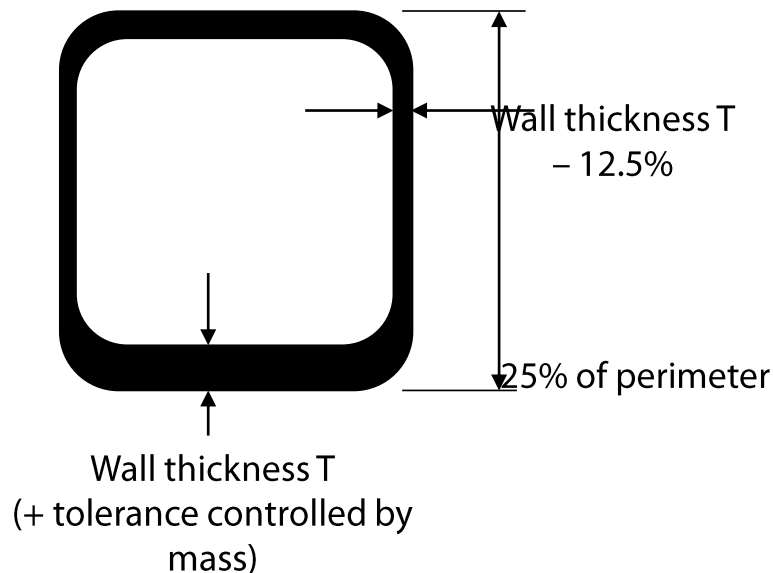


## Technical Information

The Celsius 420 is a true full body normalised hot finished structural hollow section.

It should be compared more with the seamless tube than warm and cold.

When we compare the Celsius 420 against the seamless product due to the consistent manufacture it has better tolerances. The product standard EN10210 recognises this and the Celsius has better tolerances.



- **Celsius 420®** has better control on wall thickness  
(seamless can be up to -12,5% over 25% of perimeter)
- **Celsius 420®** has a uniform wall thickness and thus a concentric “Bore”. Seamless sections may be more difficult in fabrication
- **Celsius 420®** sections have a finish similar to original strip condition whereas seamless finish is typical of a hot rolling process
- **Celsius 420®** has tighter tolerance on supplied length (0/+150mm) versus seamless (+/- 500mm)
- **Celsius 420®** has full chemical composition stated on inspection certificate

## Advantages of Celsius Compared to Seamless

Paul Watson MEng CEng MIStructE

# **Welded Joints In Tubular Steel**

Steve Whitfield Beng (Hons) CEng MIStructE

Customer Technical Services - Manager

# Overview

**1****Introduction****2****Eurocode 3 Part 1-8****3****Failure Modes****4****Examples****5****New Developments**

# Introduction





# Emirates Stadium

Long span trusses





# Gloucester Quays

Speed and simplicity of construction



## M8 Footbridge Harthill

Speed and simplicity of construction





## M8 Footbridge Harthill

Quality control



# M8 Footbridge Harthill

## Lifting



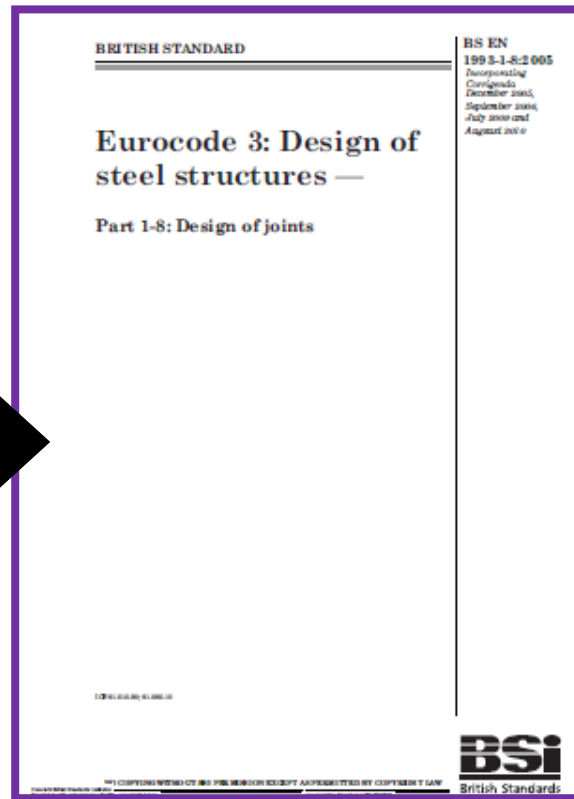
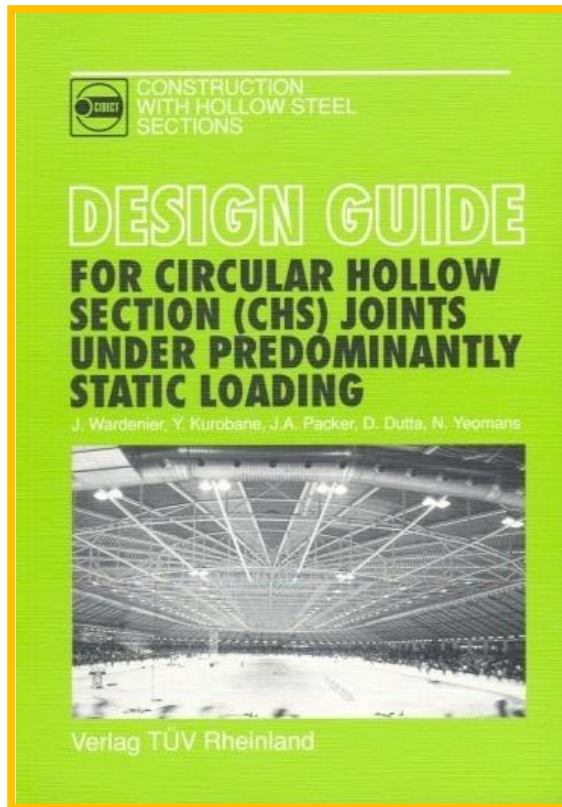
# Eurocode 3 Part 1-8





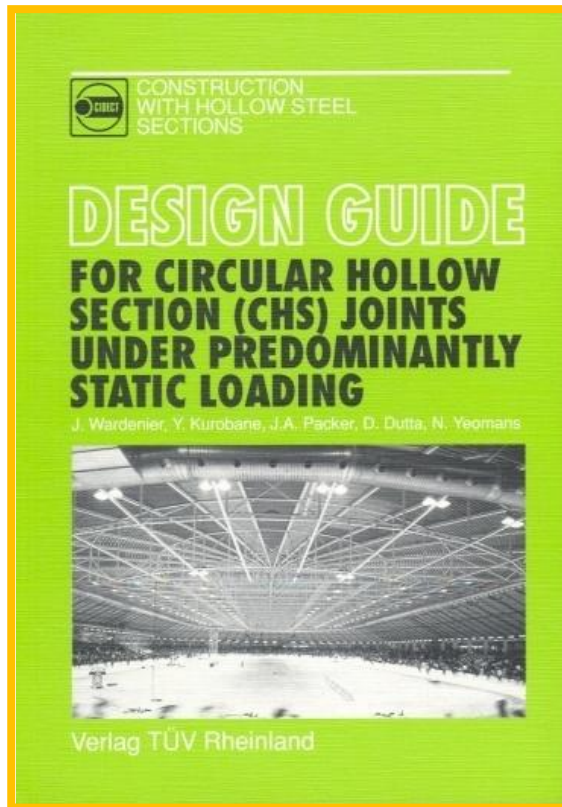
# Design Guidance

## Evolution



# Design Guidance

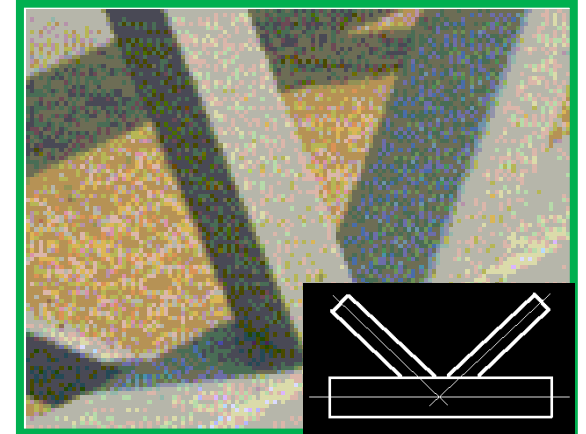
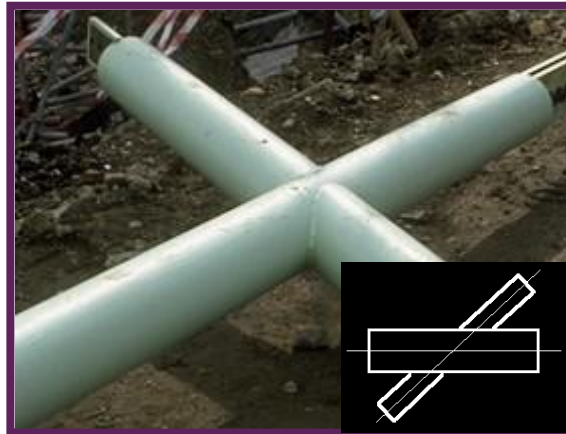
## Second Edition Cidect Design Guides





## Typical Joints

### Lattice Girders



T or Y-Joint



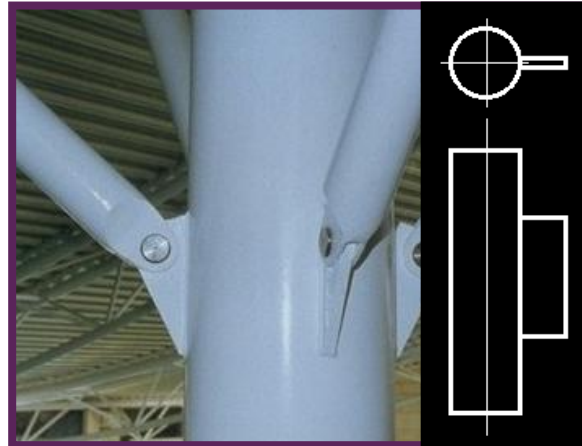
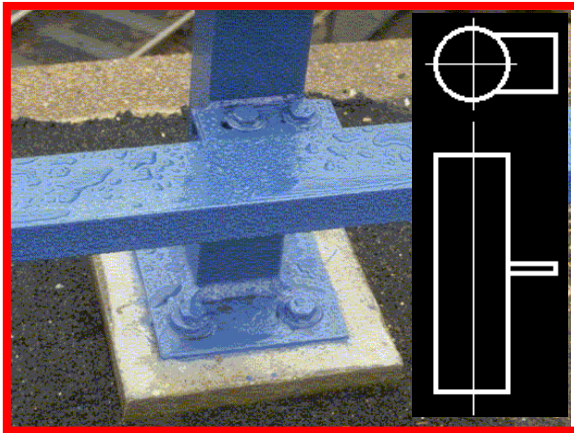
X-Joint



Gap K-Joint

## Typical Joints

### Miscellaneous



Transverse  
Gusset  
Plate



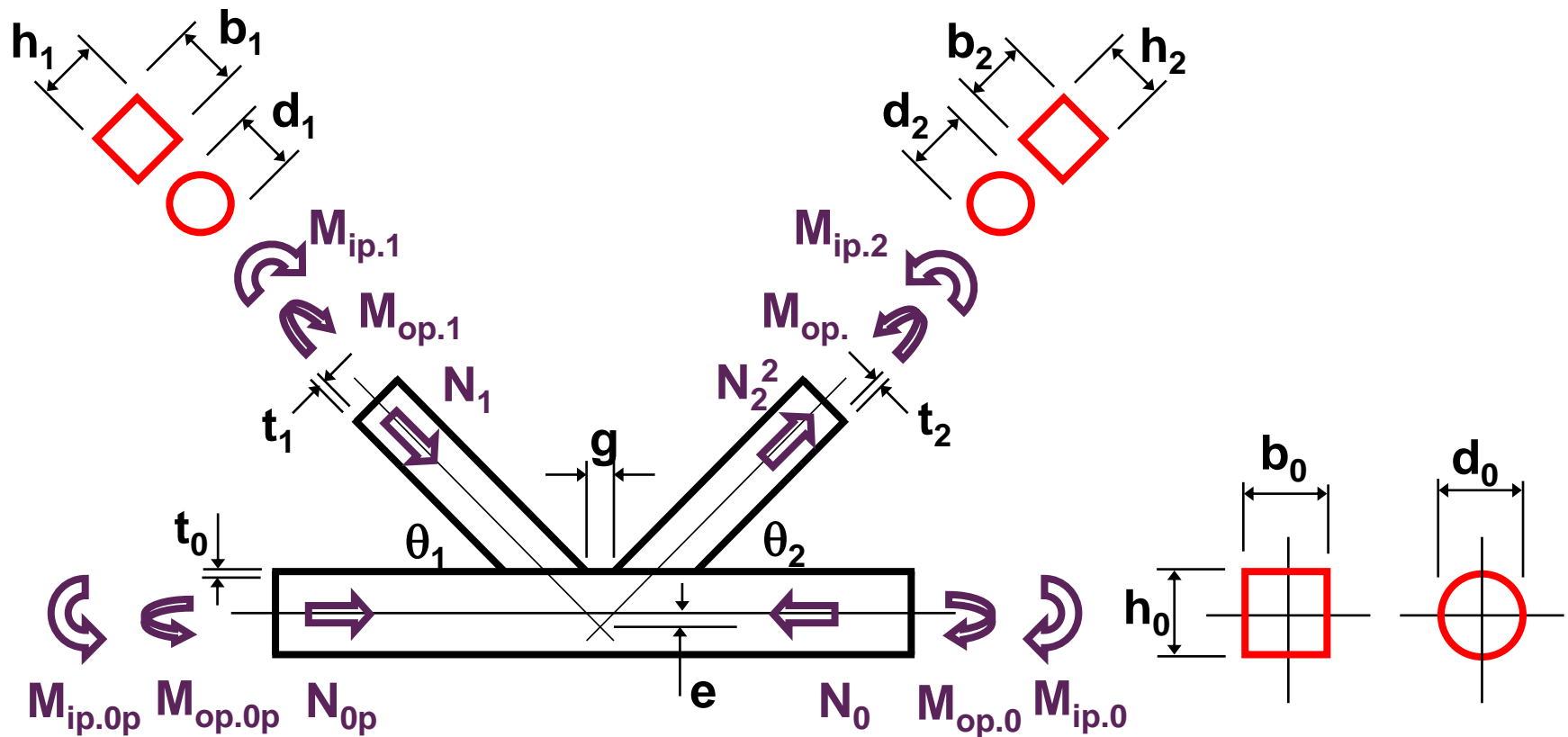
Longitudinal  
Gusset Plate



I or H Bracing

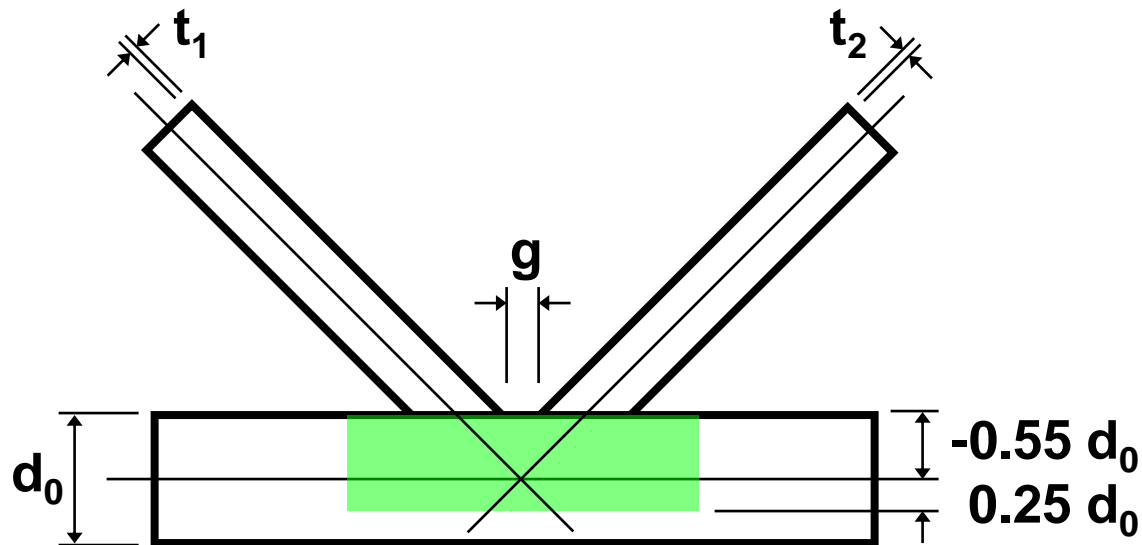
## Joint Symbols

Brace 1 usually compression brace



# Eccentricity & Effects On Geometry

## Parameters



Joint with  $e = 0$

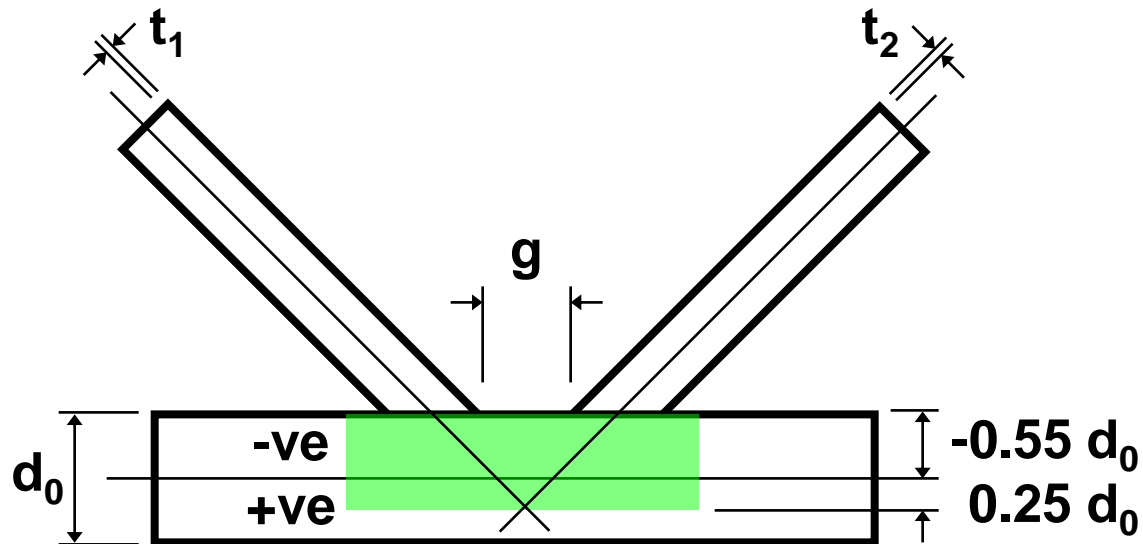
Eccentricity limit:  $-0.55 \leq e/d_0 \leq 0.25$  (shaded)

Gap limits:  $g \geq t_1 + t_2$   
 $0.5(1-\beta) \leq g/b_0 \leq 1.5(1-\beta)$

Overlap limit:  $25\% \leq Ov \leq 100\%$

## Eccentricity & Effects On Geometry

### Positive eccentricity – gap joint



Increase gap

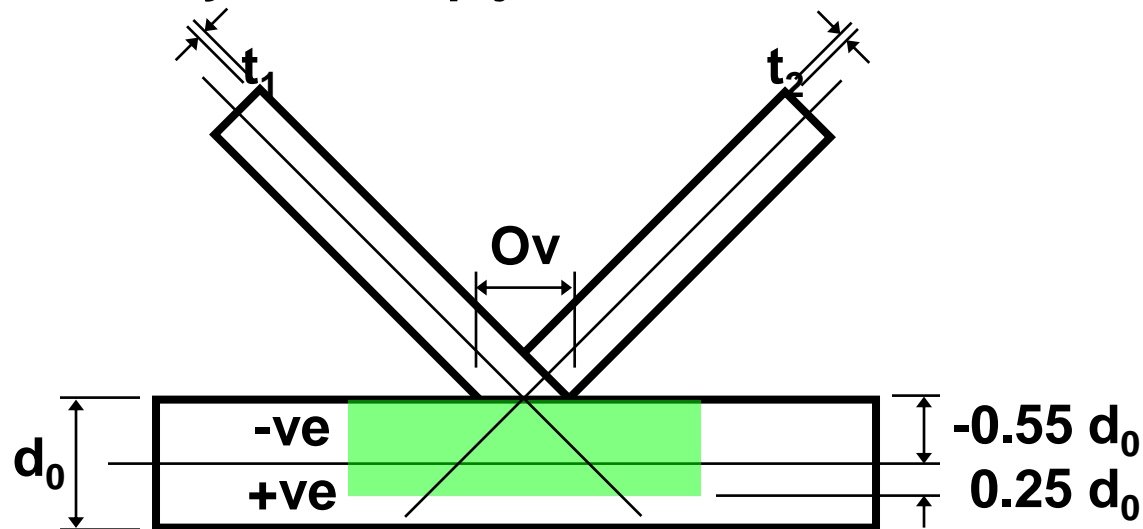
Eccentricity limit:  $-0.55 \leq e/d_0 \leq 0.25$

Gap limits:  $g \geq t_1 + t_2$   
 $0.5(1-\beta) \leq g/b_0 \leq 1.5(1-\beta)$

Overlap limit:  $25\% \leq Ov \leq 100\%$

## Joint Symbols

### Negative eccentricity – overlap joint



Overlap (100%)


Eccentricity limit:  $-0.55 \leq e/d_0 \leq 0.25$

Gap limits:  $g \geq t_1 + t_2$   
 $0.5(1-\beta) \leq g/b_0 \leq 1.5(1-\beta)$

Overlap limit:  $25\% \leq Ov \leq 100\%$

## Fabrication Costs

Bracing Handling, Cutting and Welding

Fabrication Cost	Type of Joint
	RHS chord - gap joints
	RHS chord – 100% overlap joints
	CHS chord – gap joints
	RHS chord – partial overlap joints
	CHS chord – 100% overlap joints
	CHS chord – partial overlap joints

# Laser Cutting



Repeatability

Speed



High Volume Manufacturing



Reduced Weld preparation



Versatility - Ease of assembly




Can cut bent tube



## Fabrication Costs

Bracing Handling, Cutting and Welding

Fabrication Cost	Type of Joint
	RHS chord - gap joints
	RHS chord – 100% overlap joints
	CHS chord – gap joints
	RHS chord – partial overlap joints
	CHS chord – 100% overlap joints
	CHS chord – partial overlap joints

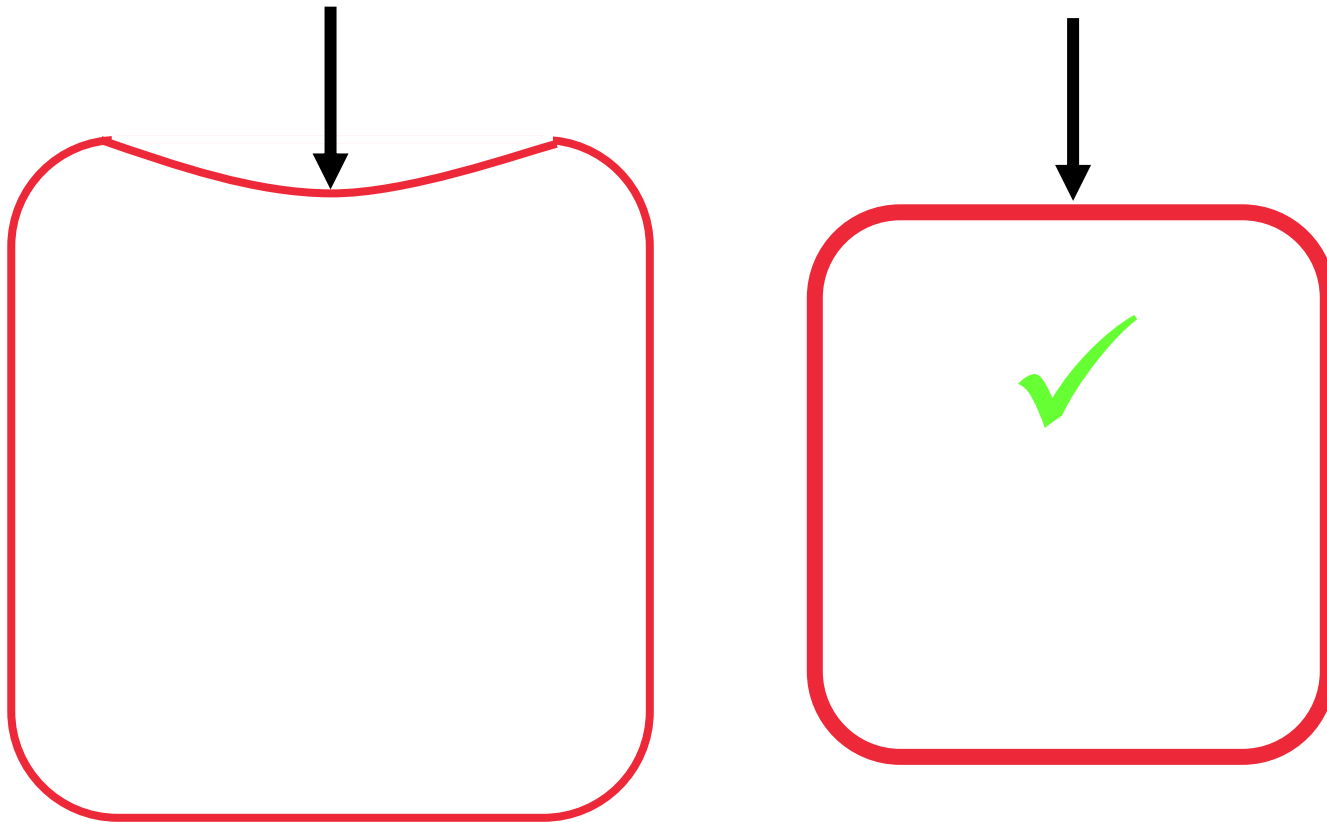
## Parameter Effects

### Gap Joints

Parameter	Direction	Effect
Chord width to thickness ratio	Down	Capacity up
Bracing to chord width ratio	Up	Capacity up
Bracing angle	Down	Capacity up
Chord factored to yield stress ratio	Less compressive	Capacity up

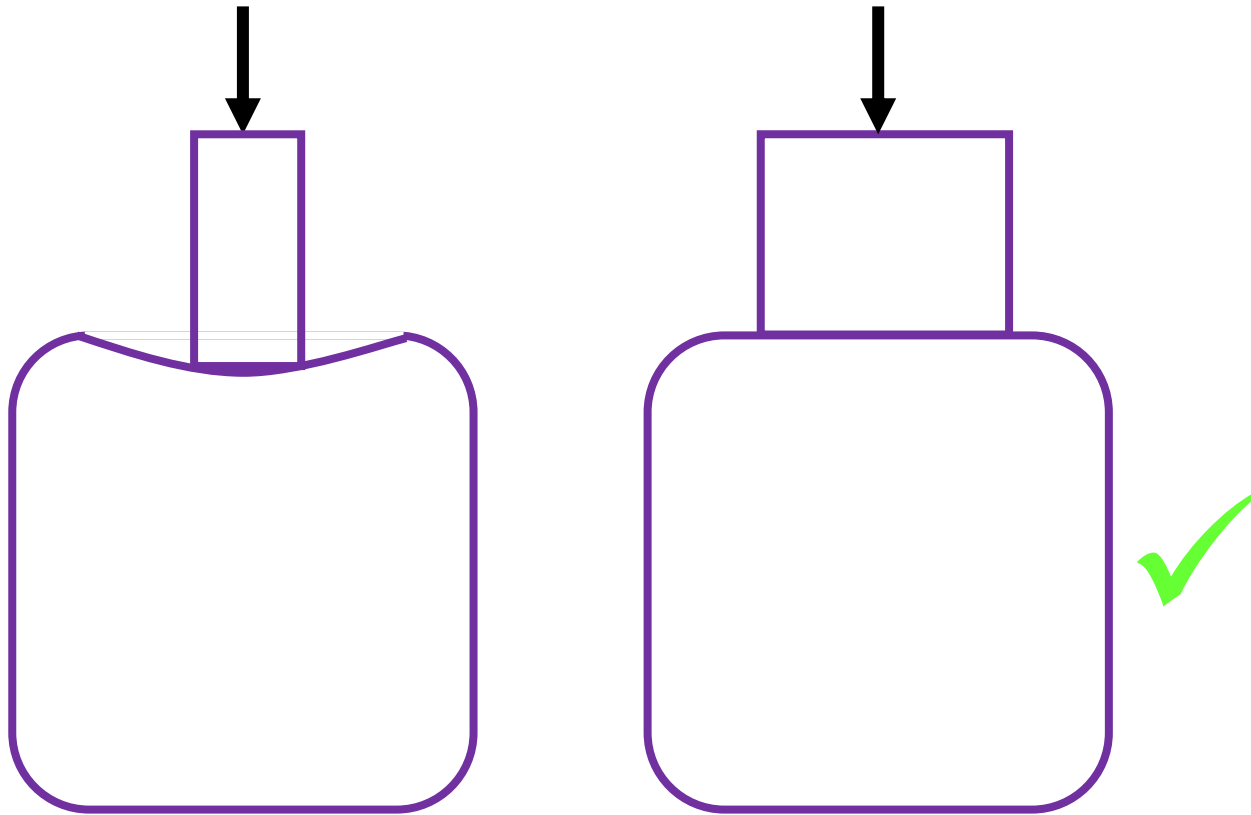
## Parameter Effects – Gap Joints

Chord width to thickness ratio



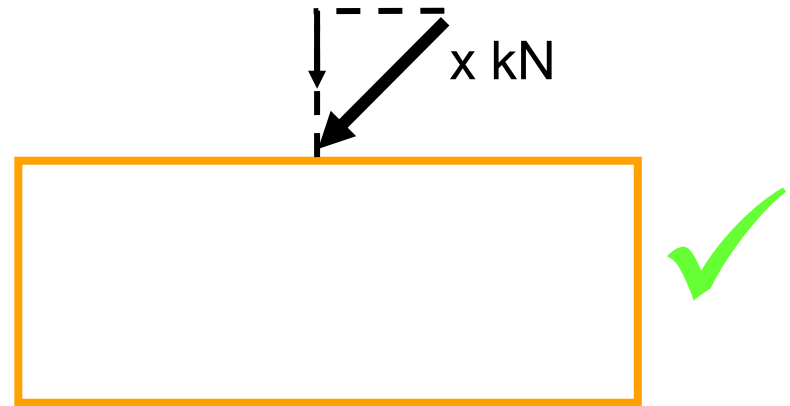
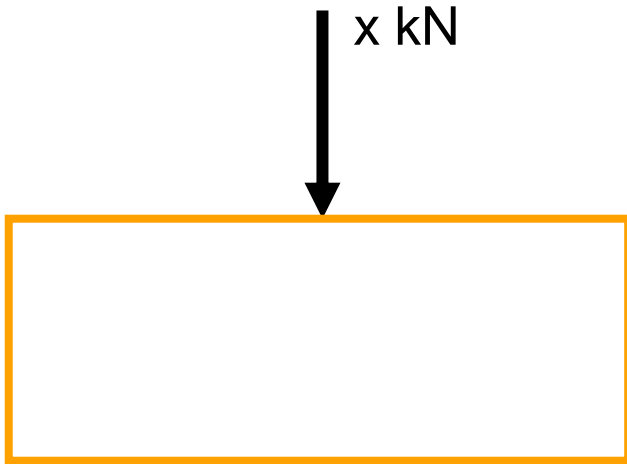
## Parameter Effects – Gap Joints

Bracing to chord width ratio



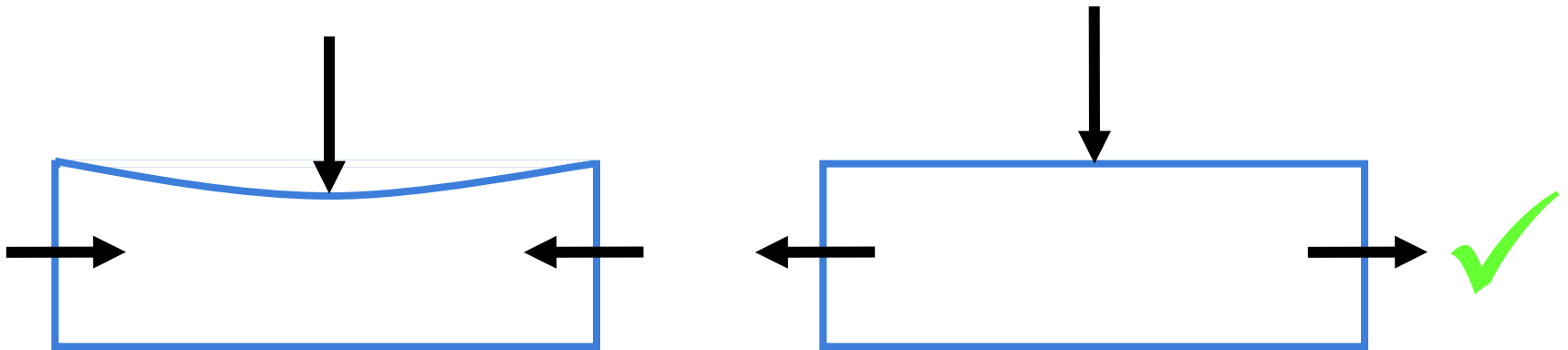
## Parameter Effects – Gap Joints

Bracing angle



## Parameter Effects – Gap Joints

Chord factored to yield stress ratio



## Parameter Effects

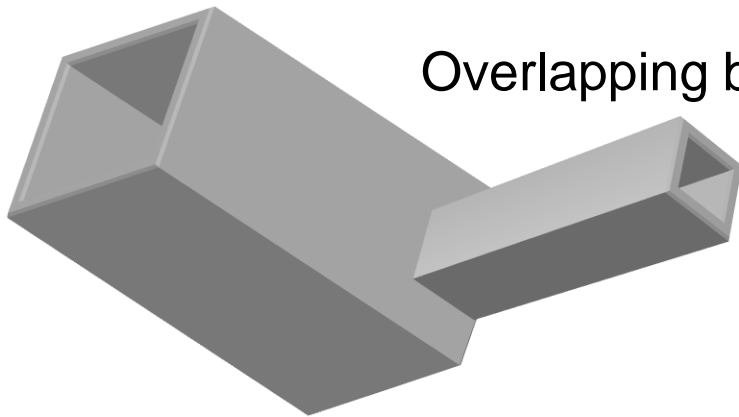
### Overlap Joints

Parameter	Direction	Effect
Chord width to thickness ratio	Down	Capacity up
<b>Bracing width ratios</b>	Down	Capacity up
<b>Overlap</b>	Up	Capacity up
Chord factored to yield stress ratio	Less compressive	Capacity up (CHS only)
Bracing angle	Down	Capacity up (CHS only)

## Parameter Effects – Overlap Joints

Bracing width ratios

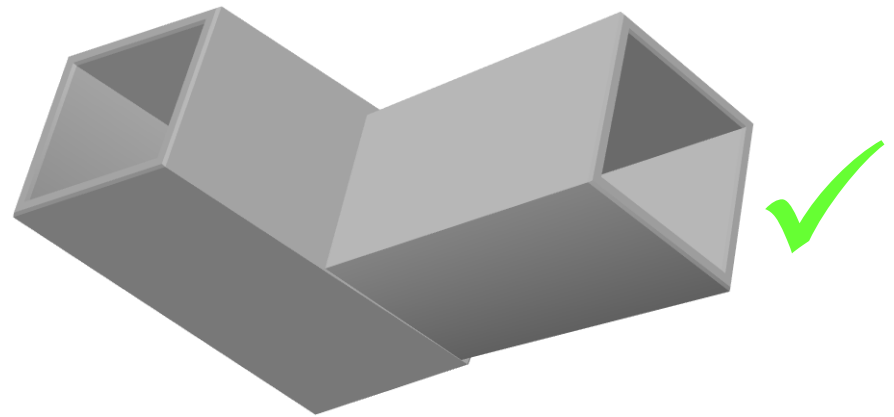
Overlapped brace



Overlapping brace

Overlapped brace

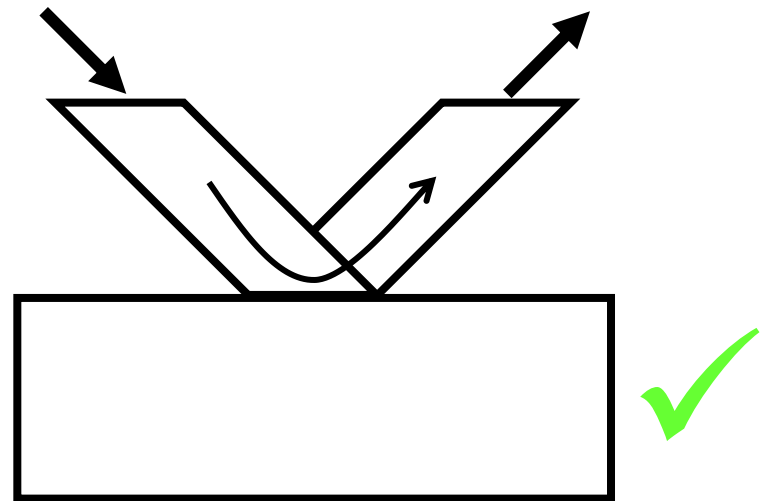
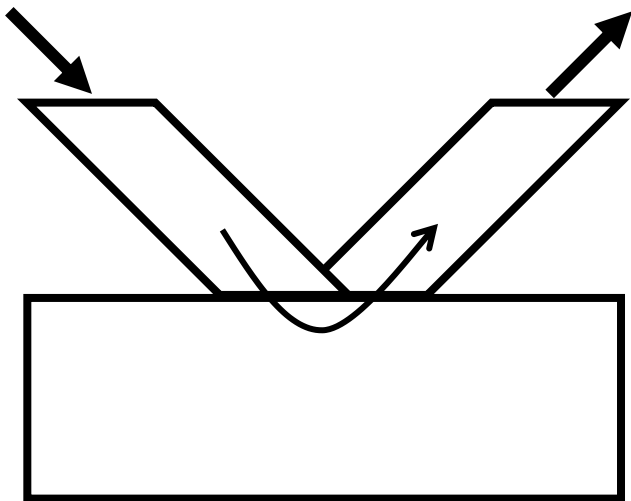
Overlapping brace



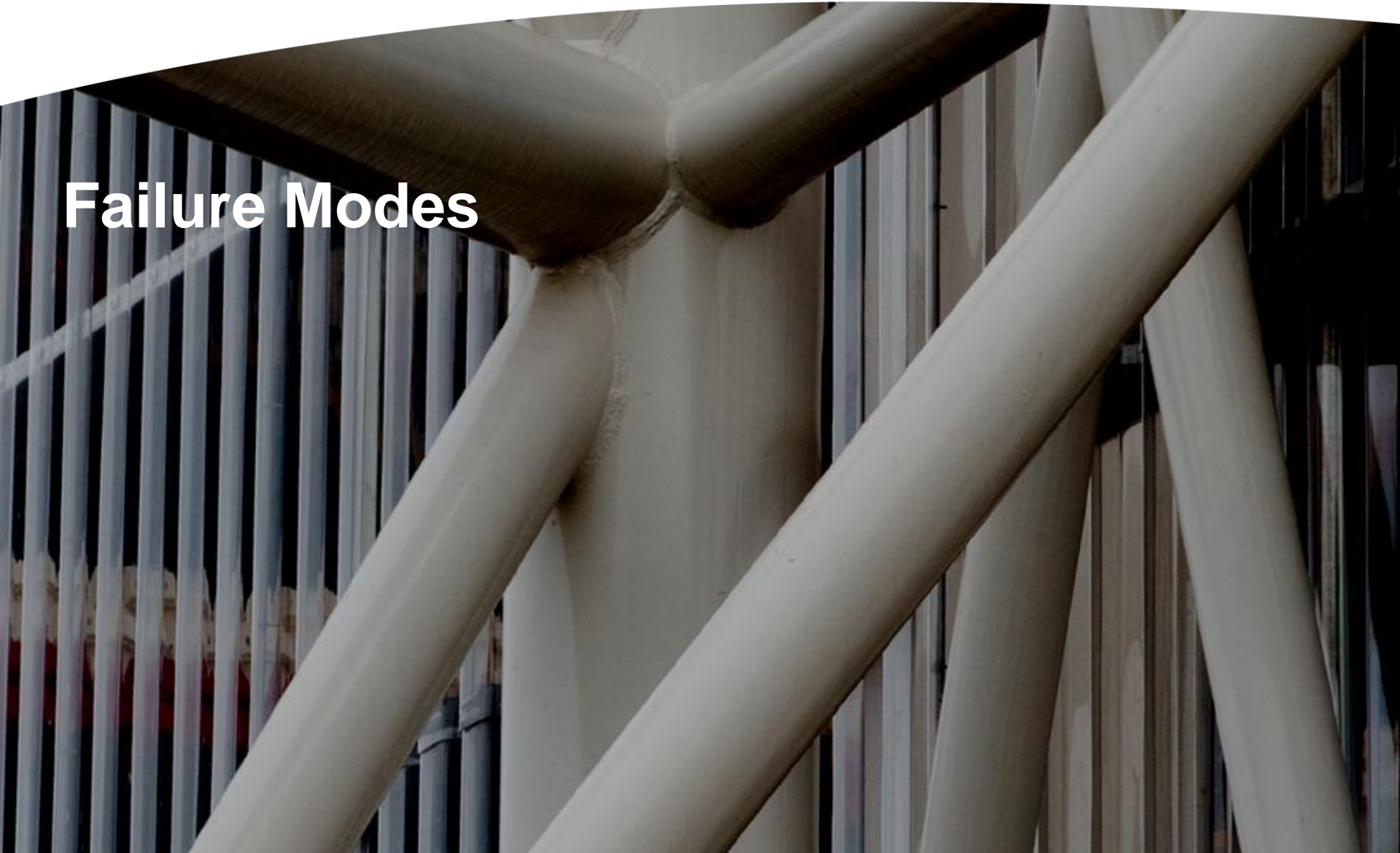


## Parameter Effects – Overlap Joints

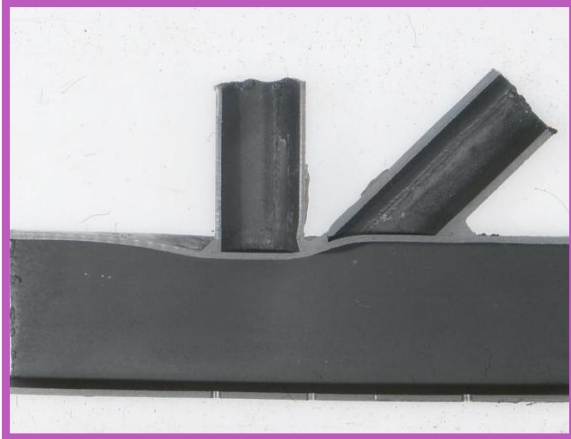
Overlap percentage



# Failure Modes



## Failure modes



Chord Face Deformation



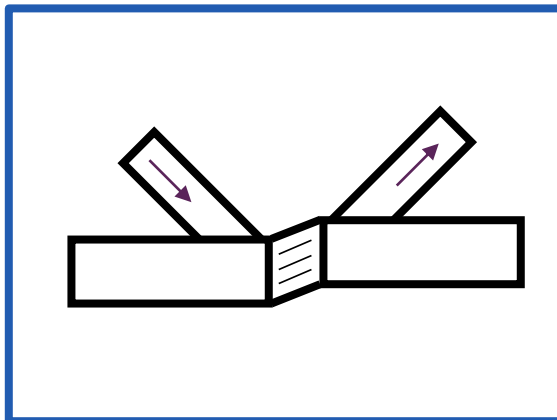
Chord Punching Shear



Chord Side Wall Buckling



Chord or brace localised buckling



Chord Shear



Bracing Effective Width

## Chord Face Deformation Failure



Also known as chord face yielding. This is the chord face deflecting under the bracing load. The formula limits the chord face deflection to 3% of the chord width as the deformation can be substantial without failing but it would not be practical to allow such deformation. Common for T, Y-joints and gap K, N-joints with the bracing to chord width ratio less than 0.85.

## Chord Punching Shear



*The chord has sheared not the weld.*

Where the bracing punches through the chord face. This occurs on the tension brace, important to realise it applies to compression and tension bracings. Shear can occur when the brace is pulling just the same as when the brace is pushing. Not usually critical but can occur when the chord width to thickness ratio is small.

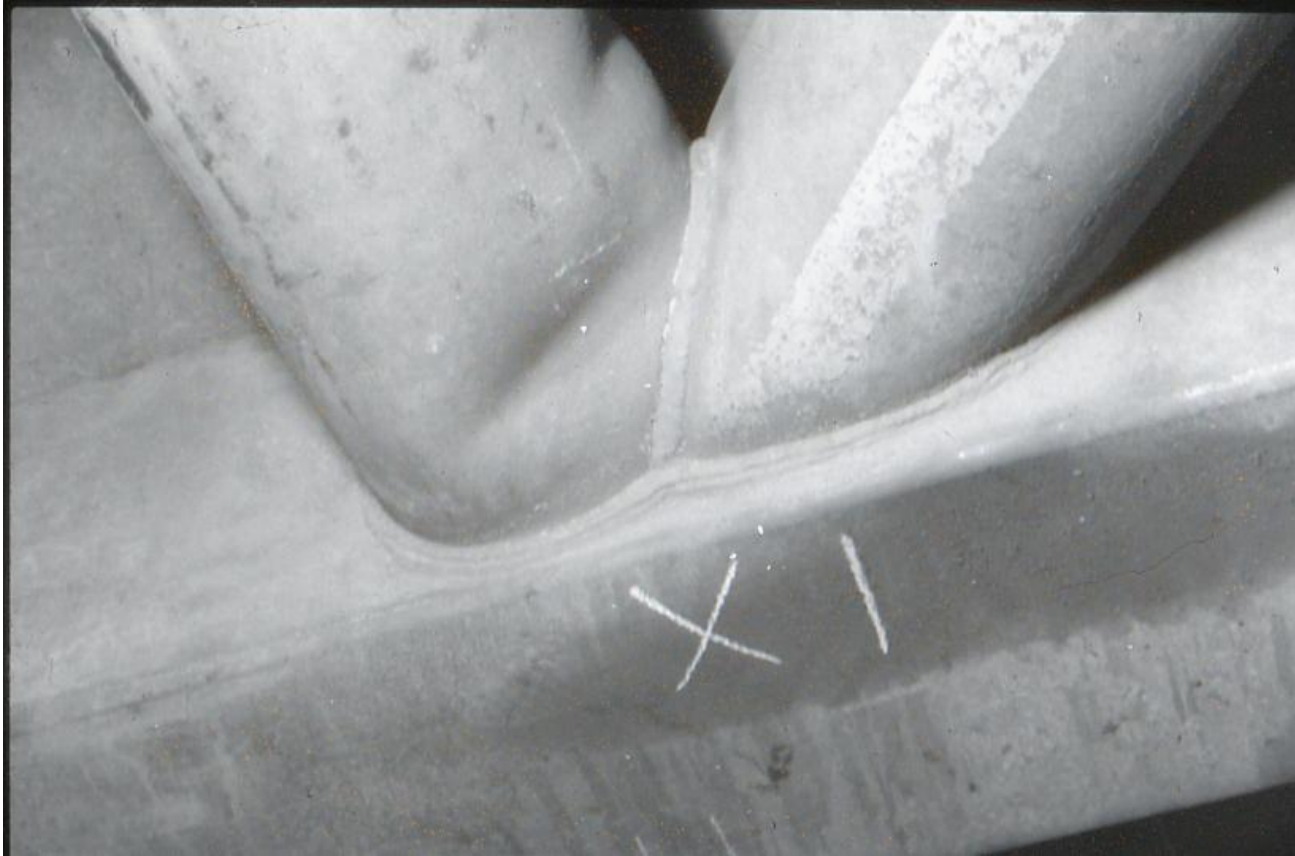


## Chord Side Wall Buckling



Typically a gap joint or single brace with beta ratio (brace width to chord width ratio)  $>0.85$  as in this example. The chord side wall under the compression brace acts as a strut and if the chord side wall is too thin and tall it will buckle under the compressive load.

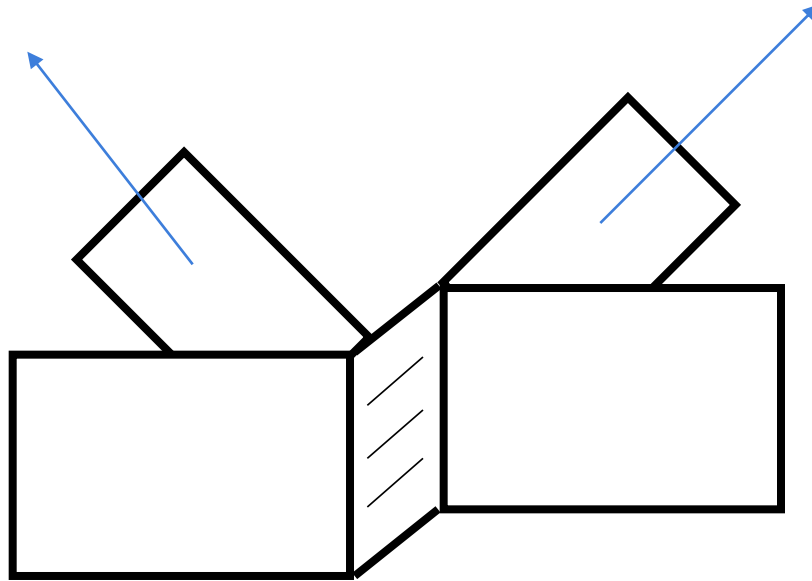
## Chord or Bracing Localised Buckling



Due to a non-uniform stress distribution at the joint but does not occur providing the joint parameters are met.

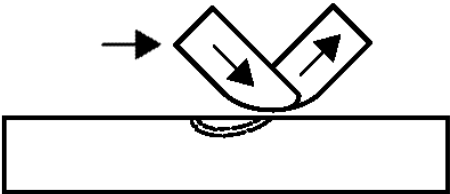


## Chord Shear



Not often critical unless RHS chords with width greater than depth are used. Does not occur for CHS joints if within parameters.

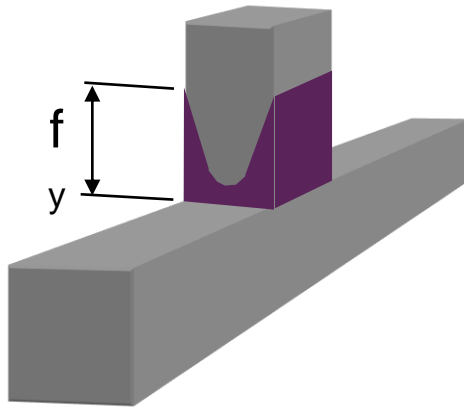
## Horizontal Shear

Mode	Description
Shear of overlapping bracings	

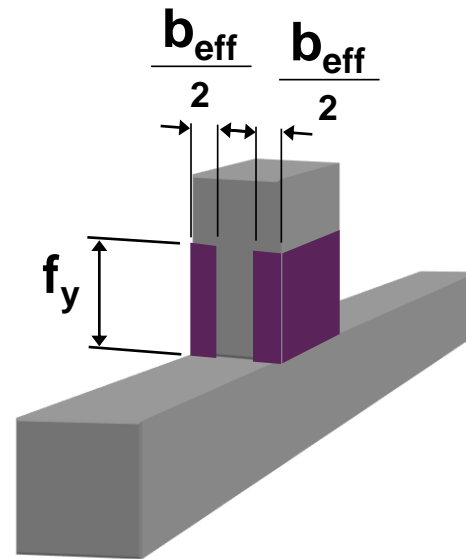
- **Local shear of overlapping bracings**, figure 17, is due to the horizontal component from the bracing forces shearing. This failure mode becomes critical for large overlaps, over 80% or 60% depending if the hidden toe of the overlapped bracing is welded to the chord

## Failure modes

### Bracing effective width RHS/SHS Chord



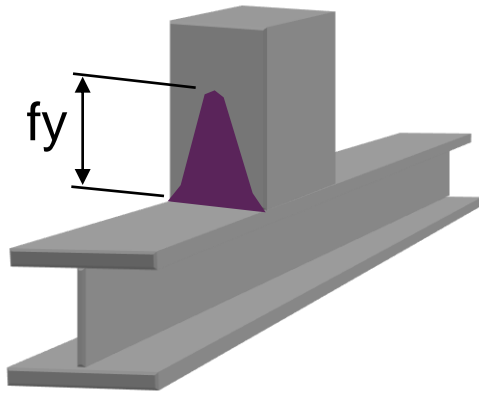
Axial stress distribution



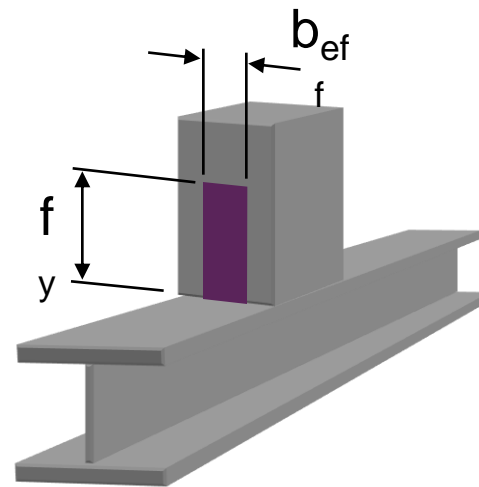
Hypothetical  
axial stress distribution

## Failure modes

Bracing effective width UB/UC Chord



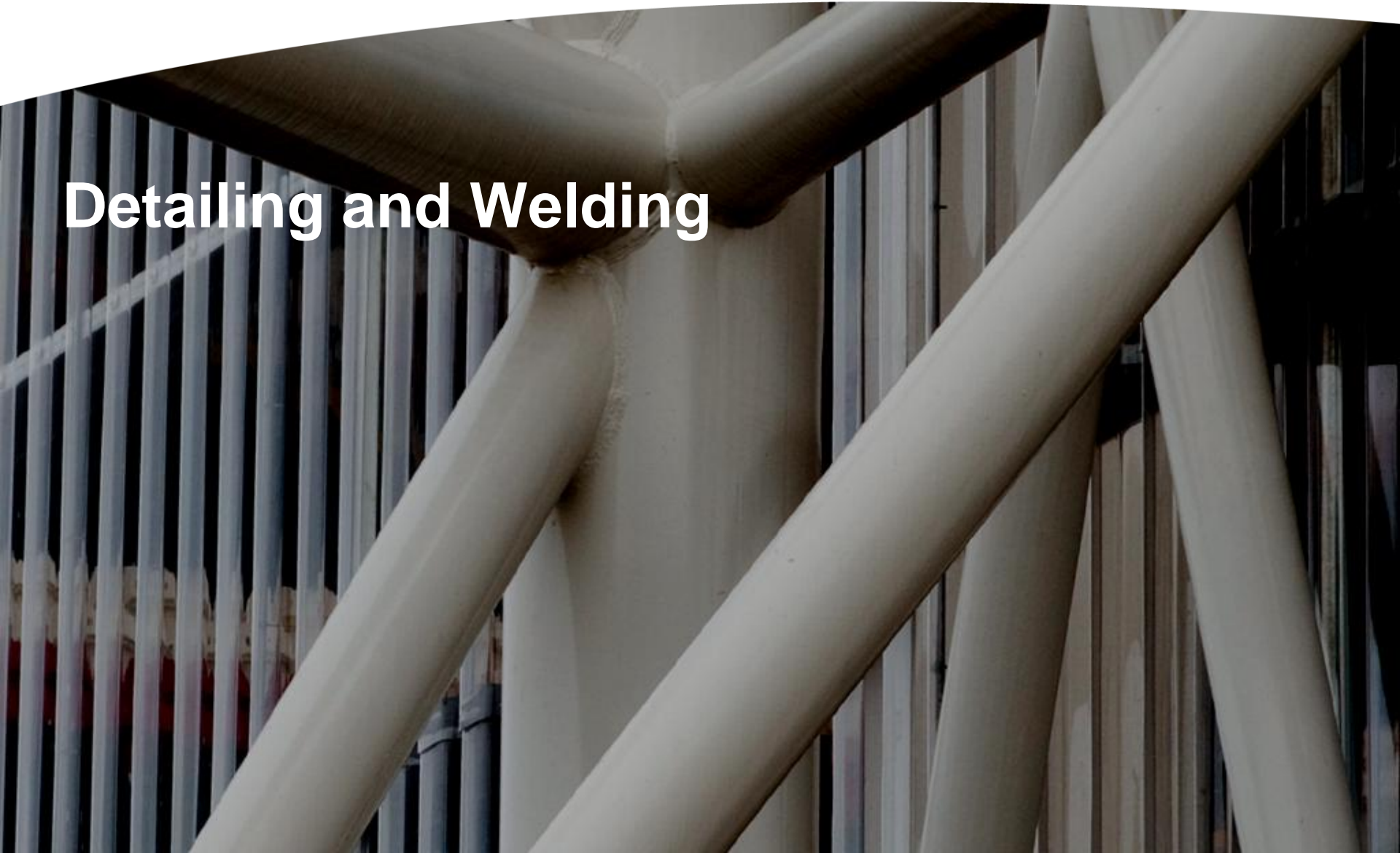
Axial stress distribution



Hyperthetical  
axial stress distribution

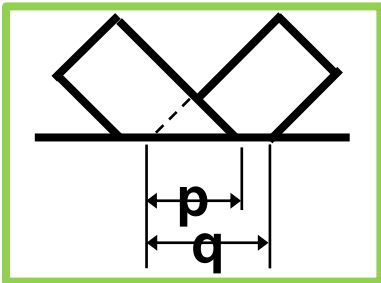


# Detailing and Welding



# Detailing

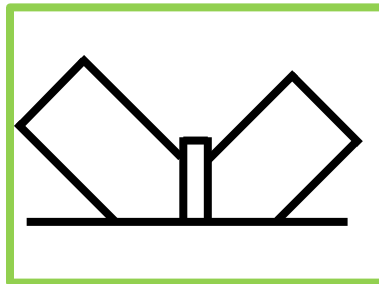
## Overlaps



- Overlap = p
- Overlap % =  $p/q \times 100$



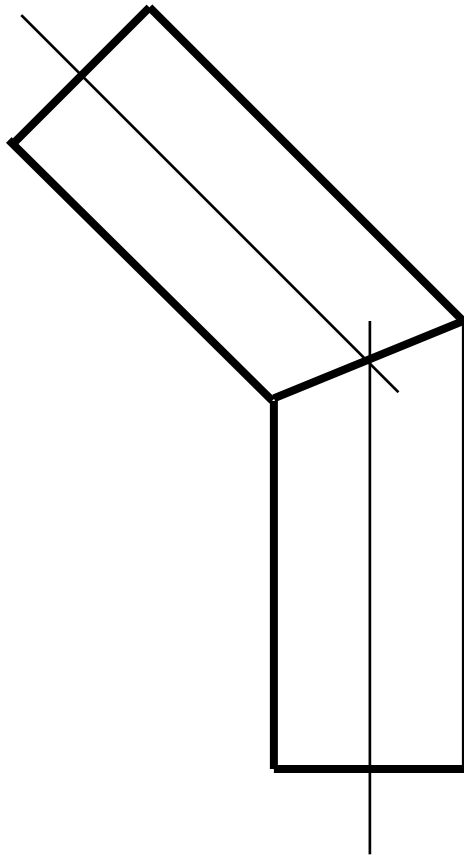
- Overlap bracings should NEVER be made like this
- Difficult to fabricate
- Up to 20% weaker



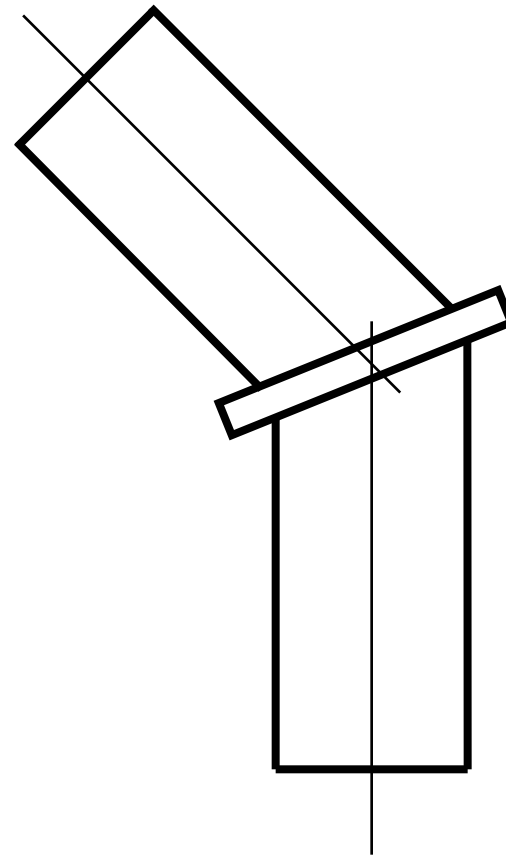
- Use division plate as alternative
- Helps to reinforce joint

## Detailing

Knee Joints



Un-reinforced Knee



Reinforced Knee

## Detailing

### Multiplanar joints





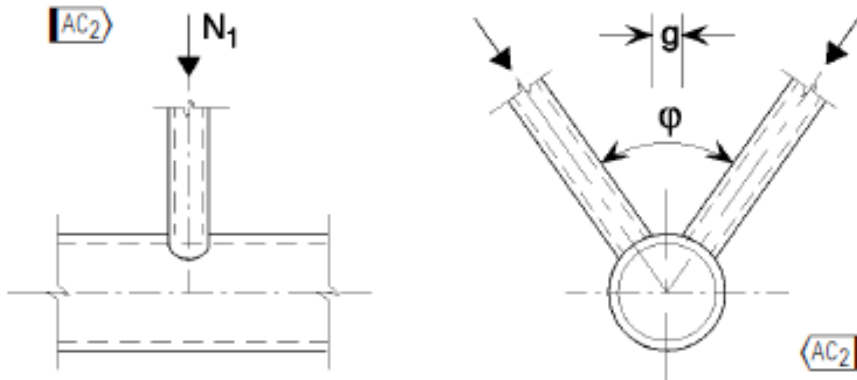
## Multiplanar Joints

### TT Joint

TT joint

$$60^\circ \leq \varphi \leq 90^\circ$$

Member 1 may be either tension or compression.



$$\mu = 1,0$$

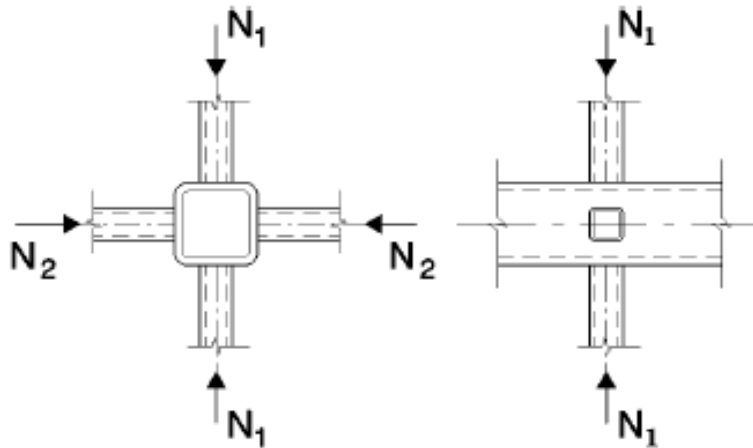
# Multiplanar Joints

## XX Joint

### XX joint

Members 1 and 2 can be either in compression or tension.  $N_{2,Ed}/N_{1,Ed}$  is negative if one member is in tension and one in compression.

AC2



AC2

$$\mu = 0,9(1 + 0,33 N_{2,Ed} / N_{1,Ed})$$

taking account of the sign of  $N_{1,Ed}$  and  $N_{2,Ed}$

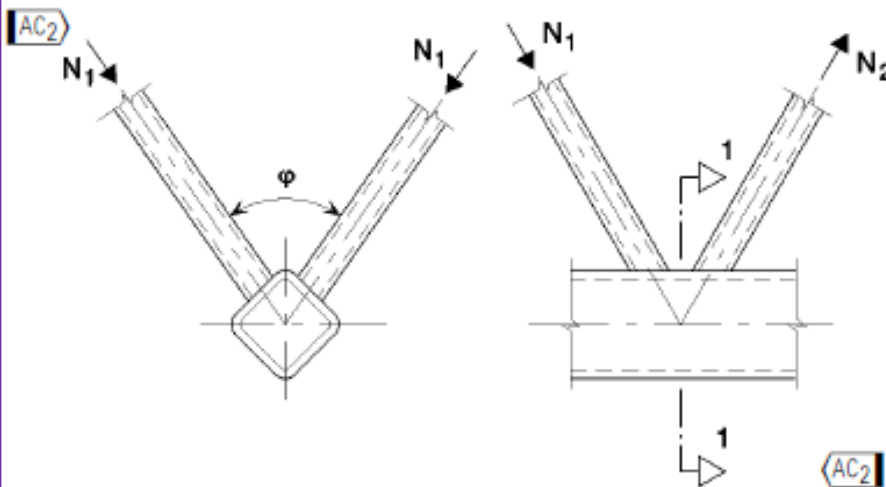
where  $|N_{2,Ed}| \leq |N_{1,Ed}|$

# Multiplanar Joints

## KK Joint

KK joint

$$60^\circ \leq \varphi \leq 90^\circ$$



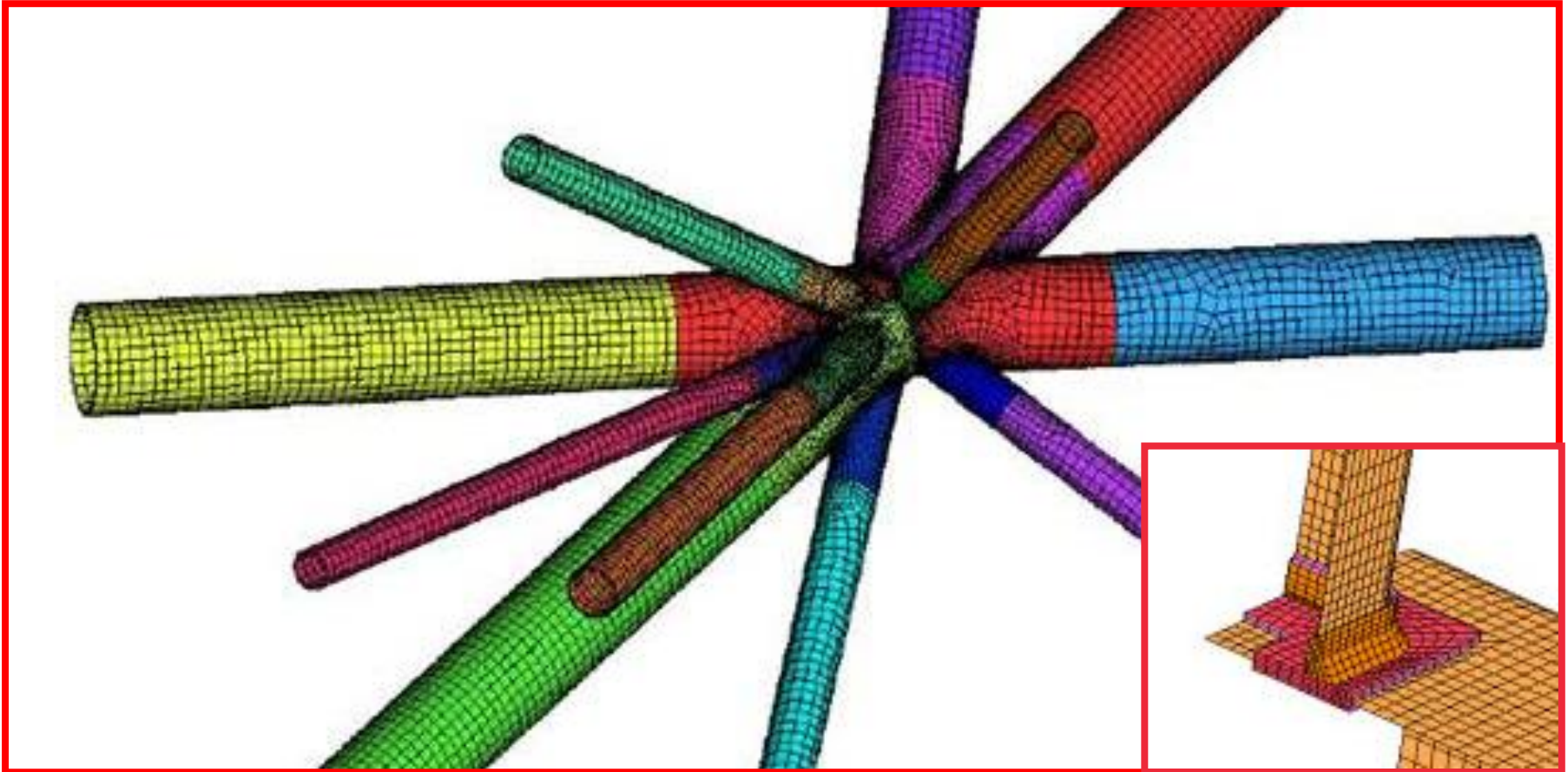
$$\mu = 0,9$$

provided that, in a gap-type joint, at section 1-1 the chord satisfies:

$$\left[ \frac{N_{0,Ed}}{N_{pl,0,Rd}} \right]^2 + \left[ \frac{V_{0,Ed}}{V_{pl,0,Rd}} \right]^2 \leq 1,0$$

# Multiplanar Joints

## Finite element modelling



# Welding

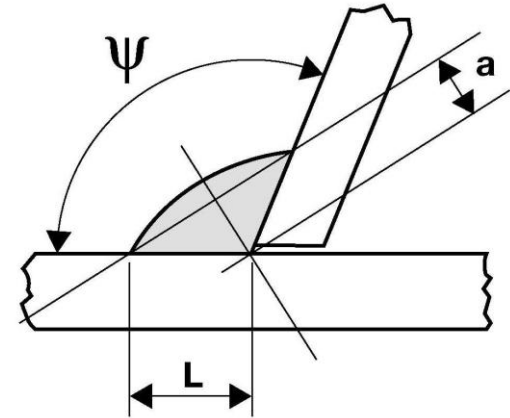
## Throat thickness



STEEL GRADE (EN10210 S355J2H)	Minimum throat size a (mm) CIDECT DESIGN GUIDE 1 & 3
CELSIUS 355	1.1 t

## Welding

Throat thickness



Leg length (l) mm	Throat thickness (a) mm
6	4.2
8	5.6
10	7.0

Elements at 90 °

# Welding

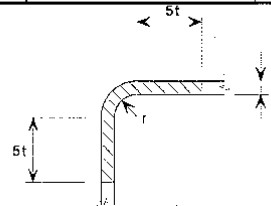
## Cold forming

### 4.14 Welding in cold-formed zones

- (1) Welding may be carried out within a length  $5t$  either side of a cold-formed zone, see Table 4.2 provided that one of the following conditions is fulfilled:
- the cold-formed zones are normalized after cold-forming but before welding;
  - the  $r/t$ -ratio satisfy the relevant value obtained from Table 4.2.

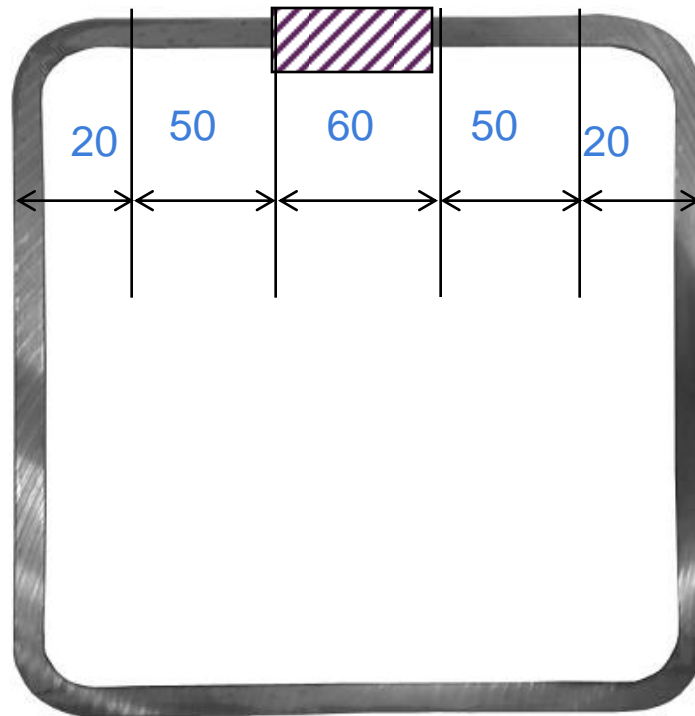
**Table 4.2: Conditions for welding cold-formed zones and adjacent material**

$r/t$	Strain due to cold forming (%)	Maximum thickness (mm)		
		Generally		Fully killed Aluminium-killed steel ( $Al \geq 0,02 \%$ )
		Predominantly static loading	Where fatigue predominates	
$\geq 25$	$\leq 2$	any	any	any
$\geq 10$	$\leq 5$	any	16	any
$\geq 3,0$	$\leq 14$	24	12	24
$\geq 2,0$	$\leq 20$	12	10	12
$\geq 1,5$	$\leq 25$	8	8	10
$\geq 1,0$	$\leq 33$	4	4	6



# Welding

Cold forming



200 x 200 x 10 CF RHS

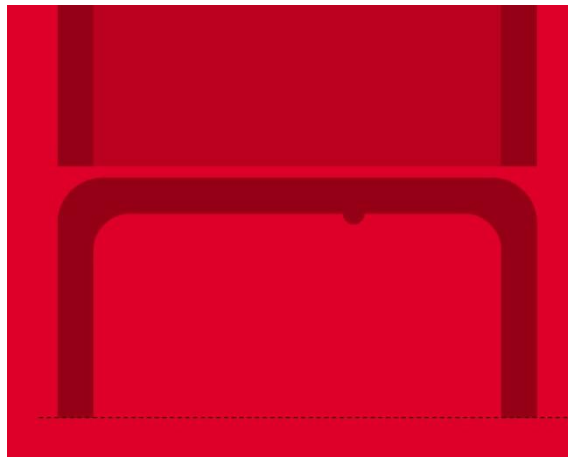
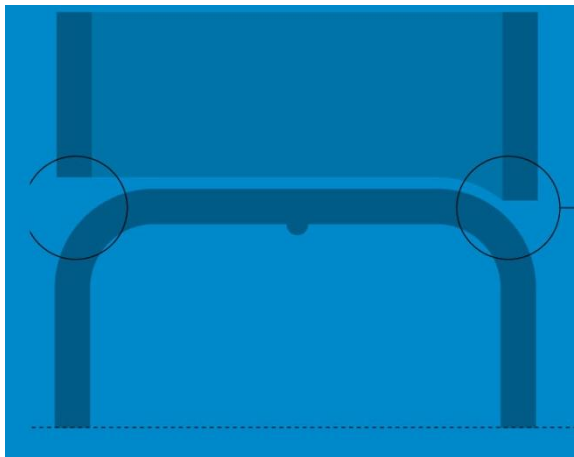


# Welding

## Cold forming

Material Standard EN10219 has the following corner radius range :-

- |                           |              |
|---------------------------|--------------|
| ▪ $T < 6 \text{ mm}$      | 1.6T to 2.4T |
| ▪ $6 \text{ mm} < T < 10$ | 2.0T to 3.0T |
| ▪ $10 < T$                | 2.4T to 3.6T |



# Joint Design Considerations

- The joint strength is determined by the selected chord and bracing member sizes, grades and geometry
- These are decided by the



# DESIGNER

## Summary

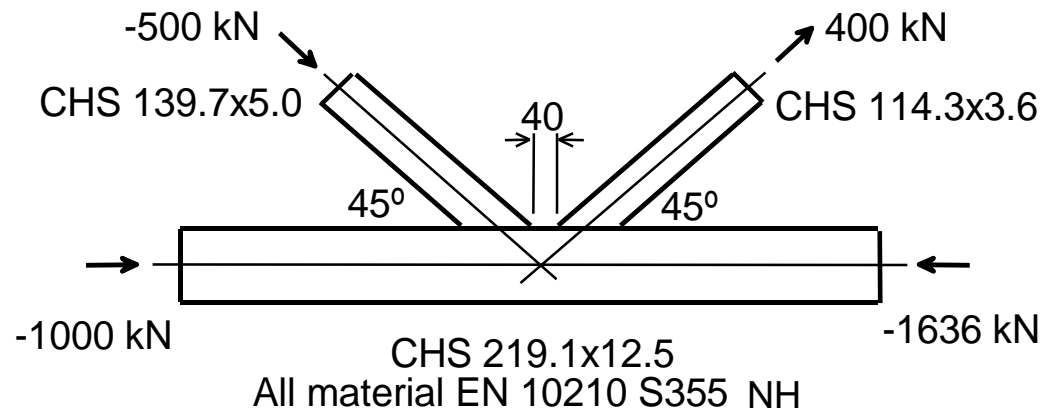
- From a compression member strength consideration , large thin wall sections are preferred (reduced  $l/r$  ratio).
- From a joint strength consideration , small thick wall chords are preferred to large thin wall chords.
- A large bracing width to chord width ratio generally increases the joint strength . This favours the use of a small thick wall chord to large thin bracing.

## Conclusion

- Joint Capacity is dependant on:
  - Brace Angle
  - Bracing Width to Chord Width Ratio
  - Chord Width to Thickness Ratio
  - Gap or Overlap Bracings
  - Chord Compressive Stress
  - Chord Yield Strength

## Joint Design Examples

### Example 1 – CHS Gap K-joint

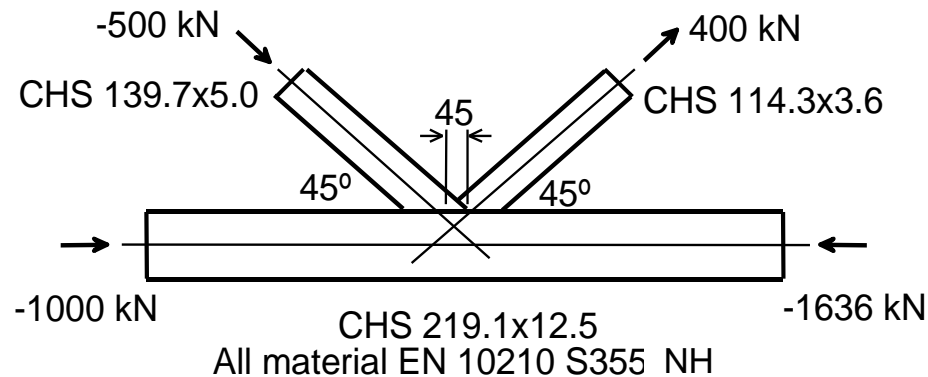


### DESIGN CHECKS :-

- Parameter Limits (5.1.1)
- Chord Face Deformation (5.1.3), *Chord End Load Function* (5.1.2)  
*Gap/Lap Function* (5.1.2)
- Chord Punching Shear (5.1.3)

## Joint Design Examples

### Example 2 – CHS Overlap K-joint



### DESIGN CHECKS :-

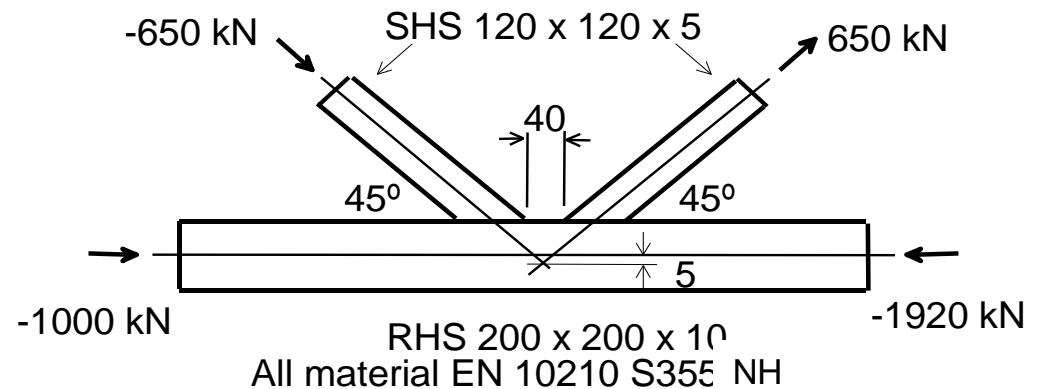
- Parameter Limits (5.1.1)
- Chord Face Deformation (5.1.3), Chord End Load Function (5.1.2)  
Gap/Lap Function (5.1.2)
- Localised shear check (if greater than 60 %)
- Chord Punching Shear (5.1.3)

## Joint Design Examples

### Example 3 – RHS Gap K-joint

#### DESIGN CHECKS :-

- Parameter Limits (5.2.1)
- Chord Face Deformation (5.2.3), *Chord End Load Function* (5.2.2)
- Chord Shear Between Bracings (5.2.3), *Chord Shear Area* (5.2.2)
- 4. Bracing Effective Width (5.2.3), *Normal Effective Width* (5.2.2)
- 5. Chord Punching Shear (5.2.3), *Normal Effective Width* (5.2.2)  
*Punching Shear Effec. Width* (5.2.2)
- 6. Chord Axial Load Resistance At Gap (5.2.3),  
*Factored Applied Shear Load In Gap* (7.1)  
*Chord Shear Capacity* (7.1)





# New Developments



## New Developments

### Tubular Joint Design Program

- Updated to include latest amendments to Eurocode 3 Part 1-8

### Concrete Filled Hollow Section

- FireSoft design software available and Design Guide for Concrete Filled Structural Hollow Section which constitutes NCCI to Eurocode 4 Part 1-2

### Fine Grained Steel

- Celsius S420 now available as EN10210 S420 NH

## Celsius 420 - Specification

Hot Finished Structural Hollow Section of Non alloy and Fine Grain Steels

# EN10210:S420 NH

Tensile Strength  
 $520\text{N/mm}^2 - 680\text{ N/mm}^2$

Minimum yield strength  
 $\leq 16\text{mm:- } 420\text{ N/mm}^2$

Minimum Impact  $-20^\circ\text{C}$  @ 40 J

Elongation - 19 %

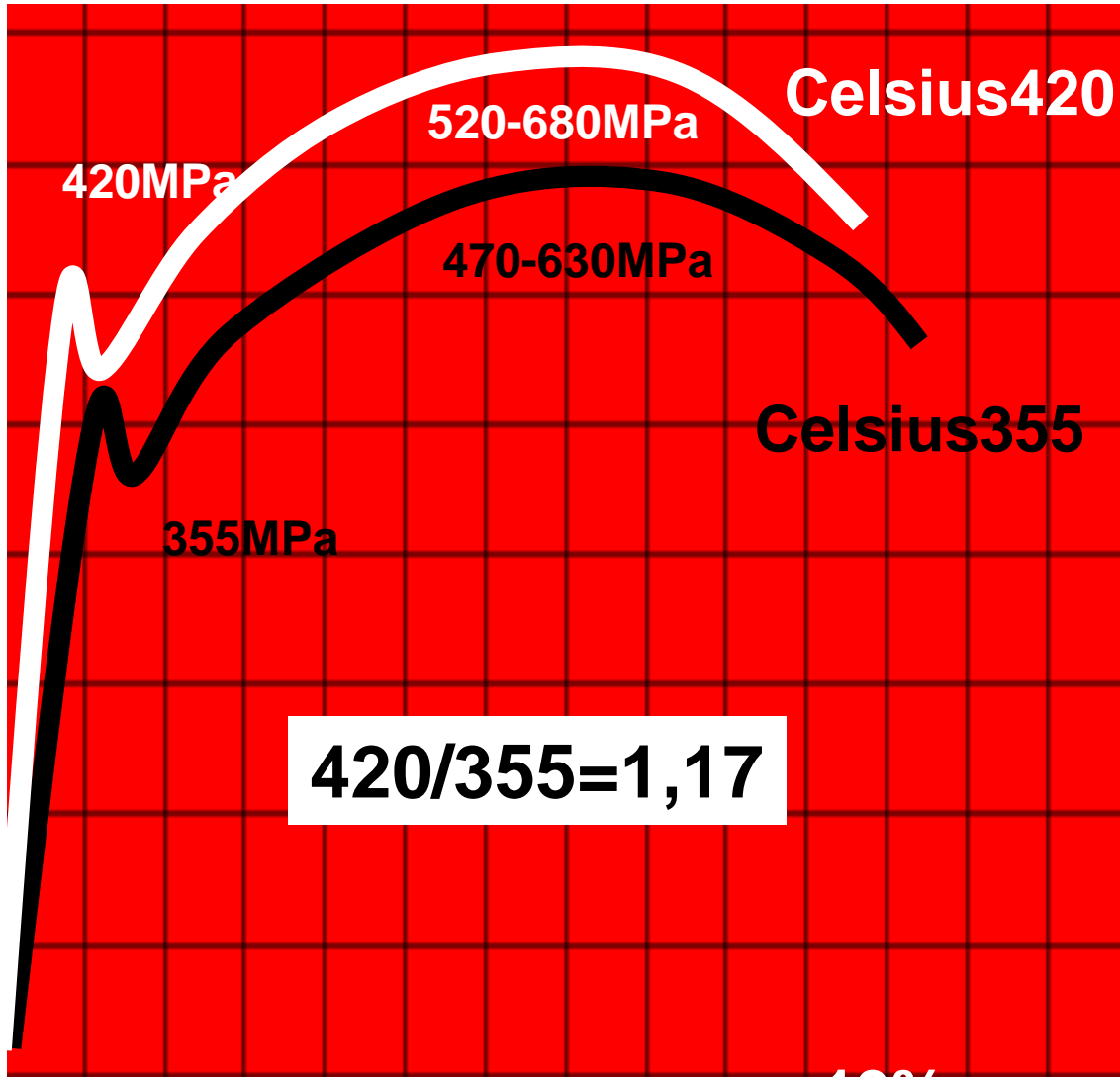
Carbon Equivalent (CEV)  
– 0.50

Silicon Content Si  
- 0.60

**Carbon Equivalent (CEV)  
Celsius 420 NH – 0.45**

**Silicon Content (Si)  
Celsius 420 NH – 0.15 to  
0.25**

## Celsius 420 - Technical Information



### ■ Yield / Ultimate

- Celsius420 starts to deform plastically (irreversible) at a higher Yield
- Celsius420 reaches a higher ultimate strength before sample fractures

## Celsius 420 - Technical Information



### ■ Celsius S355

- 200x100x10



### ■ Celsius S420

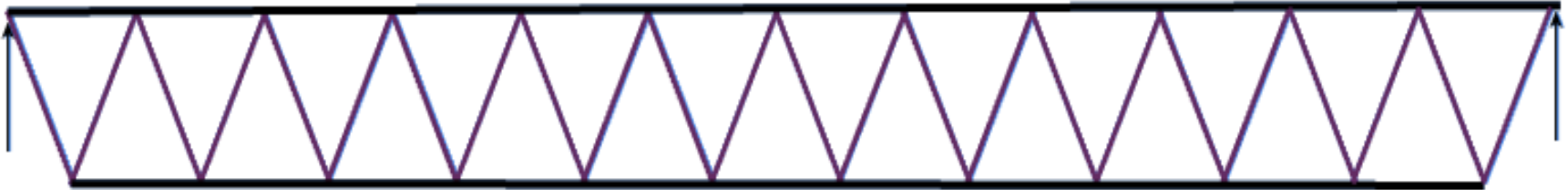
- Can make thinner/lighter
- e.g. 200x100x6.3



### ■ Celsius S420

- Or smaller
- e.g. 200x100x6.3

## Celsius 420 - Technical Information



*50 m span plain roof truss  
4m deep*

*Purlins at 4m centres, Trusses @ 15 m centres*

EN10210 S355 J2H Design  
Chord – 273 x 10 CHS  
Brace – 219.1x6.3 CHS  
Truss weight = 9.5 tonnes

Celsius EN10210 S420 NH Design  
Chord – 244.5 x 10 CHS  
Brace – 193.7x6.3 CHS  
Truss weight = 8.4 tonnes

**Weight Saving - Example**



## Celsius® 420 – Size range and offering

### Celsius® 420 - Circular Hollow Sections

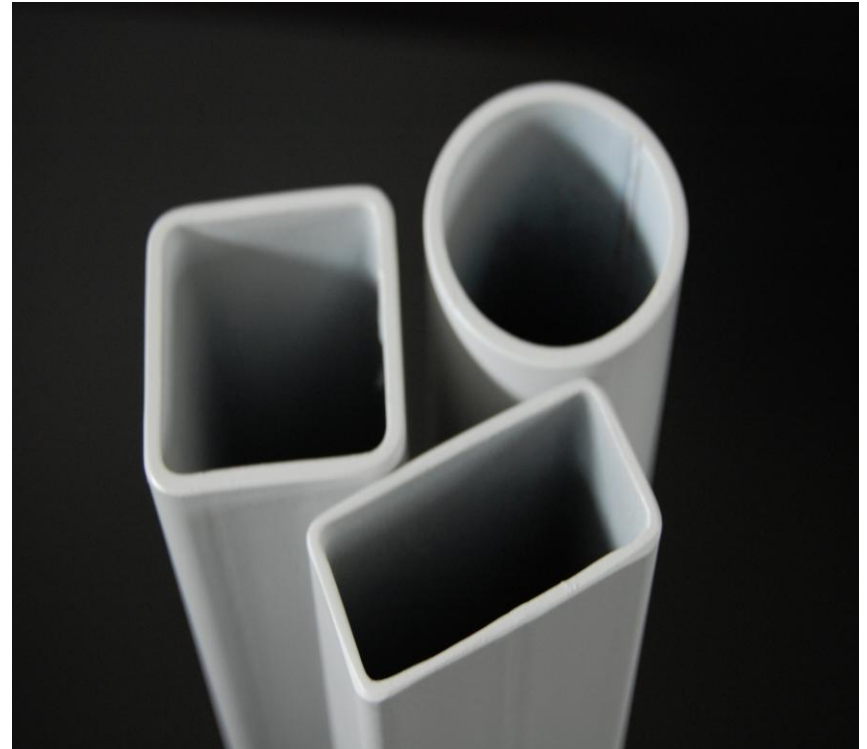
Size (mm)	2.6	2.9	3.2	3.6	4.0	4.5	5.0	6.3	8.0	10.0
21.3										
26.9										
33.7										
42.4										
48.3										
60.3										
76.1										
88.9										
101.6										
114.3										
139.7										
168.3										
193.7										
219.1										
244.5										
273.0										
323.9										
355.6										



## Celsius® 420 – Size range and offering

### Celsius® 420 - Square Hollow Sections

Size (mm)	3.0	3.2	3.6	4.0	5.0	6.3	8.0	10.0	12.5
40 x 40									
50 x 50									
60 x 60									
70 x 70									
80 x 80									
90 x 90									
100 x 100									
120 x 120									
140 x 140									
150 x 150									
160 x 160									
180 x 180					r				
200 x 200									
220 x 220									
250 x 250									
260 x 260						r			
300 x 300									
350 x 350									
400 x 400									



# Celsius® 420 – Size range and offering

## Celsius® 420 - Rectangular Hollow Sections

Size (mm)	3.0	3.2	3.6	4.0	5.0	6.3	8.0	10.0	12.5
50 x 30									
60 x 40									
80 x 40									
90 x 50									
100 x 50									
100 x 60									
120 x 60									
120 x 80									
150 x 100									
160 x 80									
180 x 60									
180 x 100									
200 x 100									
200 x 120									
200 x 150									
220 x 120									
250 x 100									
250 x 150									
250 x 200									
260 x 140									
260 x 180									
300 x 100									
300 x 150									
300 x 200									
300 x 250									
350 x 150									
350 x 250									
400 x 120									
400 x 150									
400 x 200									
400 x 300									
450 x 250									
500 x 200									
500 x 300									



## Celsius® 420 - Elliptical Hollow Sections

Size (mm)	4.0	5.0	6.3	8.0	10.0
150 x 75					
200 x 100					
250 x 125					
300 x 150					
400 x 200					
500 x 250					

r = External corner radius >2T but <3T

# Celsius® – Additional Tools

## Tube Element Design Package

**Tata Steel Tubes Element Design**

File Edit View History Bookmarks Options Window Help

Contents

My Default Tables

- Tubular Products
  - Section properties
  - Effective section properties
  - Axial compression
  - Bending moment
    - Celsius® CHS, S420 / Celsius® 420
    - Celsius® SHS, S420 / Celsius® 420**
    - Celsius® RHS, S420 / Celsius® 420
    - Celsius® CHS, S355 / Celsius® 355 D-103
    - Celsius® SHS, S355 / Celsius® 355 D-108
    - Celsius® RHS, S355 / Celsius® 355 D-112
    - Celsius® EHS, S355 / Celsius® 355 D-119
    - Hybox® CHS, S355 / Hybox® 355 D-120
    - Hybox® SHS, S355 / Hybox® 355 D-123
    - Hybox® RHS, S355 / Hybox® 355 D-126
  - Web bearing and buckling
  - Axial force and bending
  - Notes
  - Tolerances

Celsius® SHS, Bending moment. Design moment resistance and design shear resistance for Celsius® 420

EC3 Celsius® SHS Bending moment

Design moment resistance and design shear resistance  
Table 1 of 2. Range: 40x40 - 150x150  
Quick navigation

Hot Finished

EN 1993-1-1: 2005, EN 10210-2: 2006, N/Annex: UK S420 / Celsius® 420

Section Designation		Mass per Metre	Classification	Moment Resistance	Shear Resistance	Second Moment of Area
h x h	t	kg/m		$M_{c,Rd}$ kNm	$V_{c,Rd}$ kN	$I$ cm <sup>4</sup>
mm	mm					
40 x 40	3.0 #	3.41	1	2.51	52.6	9.78
	3.2	3.61	1	2.64	55.8	10.2
	3.6 #	4.01	1	2.89	61.8	11.1
	4.0	4.39	1	3.12	67.8	11.8
	5.0	5.28	1	3.64	81.6	13.4
50 x 50	3.0 #	4.35	1	4.07	67.2	20.2

To assist Engineers in the design using Celsius®.  
For software download from –  
<http://www.tatasteeleurope.com/en/products-and-services/long/tubes/technical-response-documents>

Commercial enquiries –  
[commercialcelsius420@tatasteel.com](mailto:commercialcelsius420@tatasteel.com)

Technical enquiries –  
[technicalcelsius420@tatasteel.com](mailto:technicalcelsius420@tatasteel.com)

# **Tata Steel Europe, Tubes**

**Steve Whitfield Beng (Hons) CEng MIStructE**  
**Customer Technical Services - Manager**



## Concrete Filled Hollow Sections

Wellcome Trust - London



## SHS Joint Design References

- EUROCODE No. 3: EN 1993-1-8:2005 – with national annex
  - Corrigenda 2 was issued September 2006
    - Final CEN corrigenda added February 2010
  - Similar rules to Annex K (1992) except symbols changed but the major equations remain the same.
    - Eg: End load function  $f_n$  now  $k_p$
    - Joint partial safety factor with UK NA
      - *Annex K :- Formula  $\times 1.10/\gamma_{Mj}$  where  $\gamma_{Mj} = 1.10$*
      - *EC3-1-8 :- Formula  $/\gamma_{M5}$  where  $\gamma_{M5} = 1.00$*

